



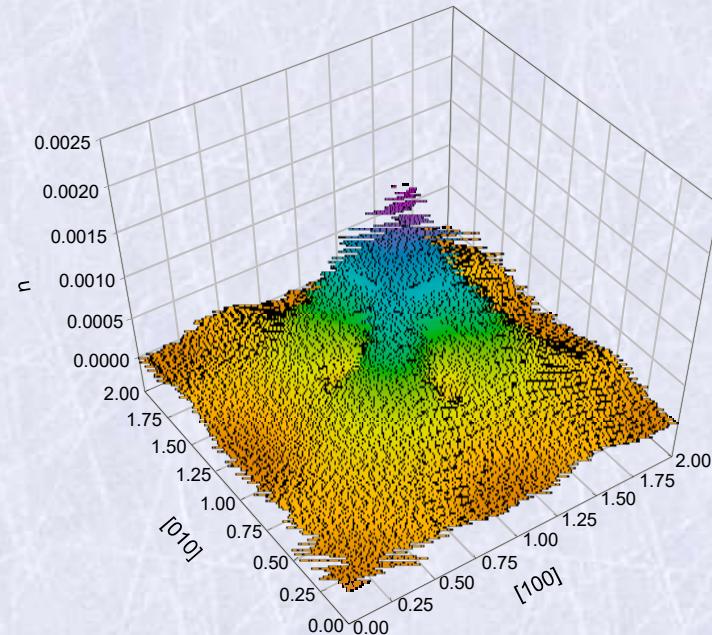
# Defects in solids

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## Outline

- lattice defects
- PAS experiment
- trapping model
- vacancies
- vacancy clusters
- dislocations





## Characterization of lattice defects in metallic materials by positron annihilation spectroscopy: A review



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Dislocations

Precipitates

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### ABSTRACT

Positron is an excellent probe of lattice defects in solids. A thermallized positron delocalized in lattice can be trapped at open volume defects, e.g. vacancies, dislocations, grain boundaries etc. Positron annihilation spectroscopy is a non-destructive technique which enables characterization of open volume lattice defects in solids on the atomic scale. Positron lifetime and Doppler broadening of annihilation photo-peak are the most common observables related to positron annihilation process. Positron lifetime spectroscopy enables to identify defects in solids and to determine their concentrations while coincidence measurement of Doppler broadening provides information about local chemical environment of defects. This article provides a review of the state-of-art of defect characterization in bulk metallic materials by positron annihilation spectroscopy. Advanced analysis of positron annihilation data and recent developments of positron annihilation methodology are described and discussed on examples of defect studies of metallic materials. Future development in the field is proposed as well.

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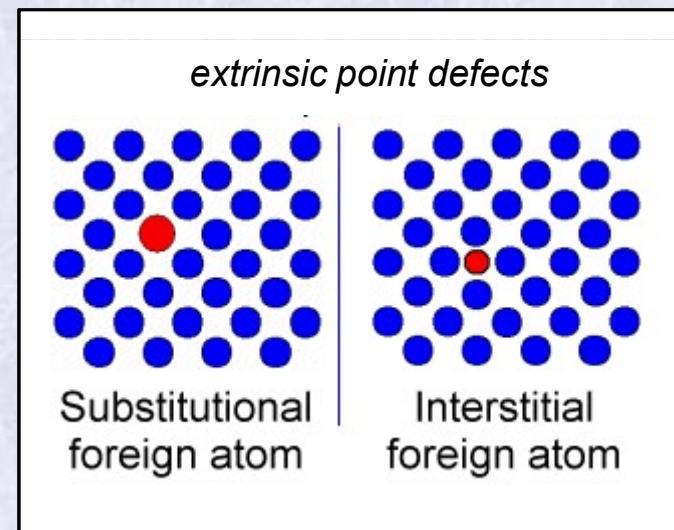
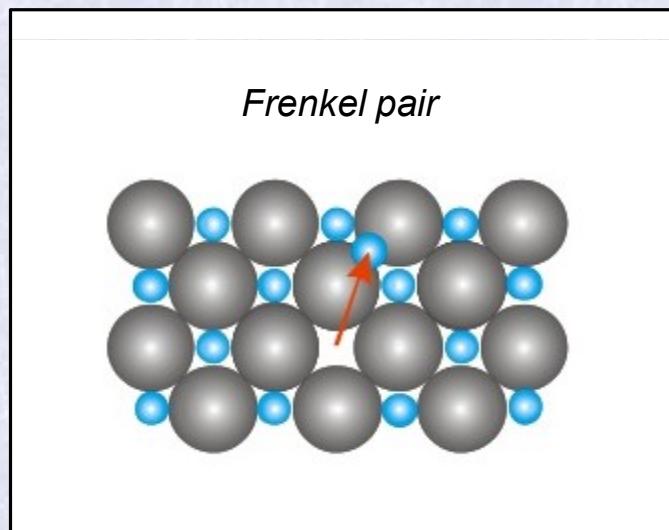
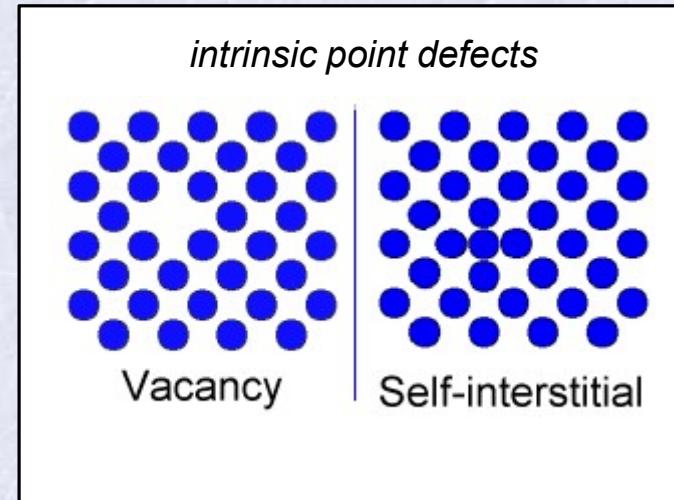
### 1. Introduction

Open volume defects of crystallite lattice, e.g. vacancies, dislocations, grain boundaries etc., have a strong influence on many physical properties of metallic materials. For example vacancies play the key role in diffusion processes [1] and phase transforma-

- (ii) The design of hardenable Al-Si-Mg based (6xxx series) alloys by micro-alloying with elements having a high binding energy with vacancies [8–10]. This way one can control natural ageing of Al-Si-Mg alloys and also the strengthening effect during subsequent artificial ageing.
- (iii) The enhancement of the equilibrium concentration of vacan-

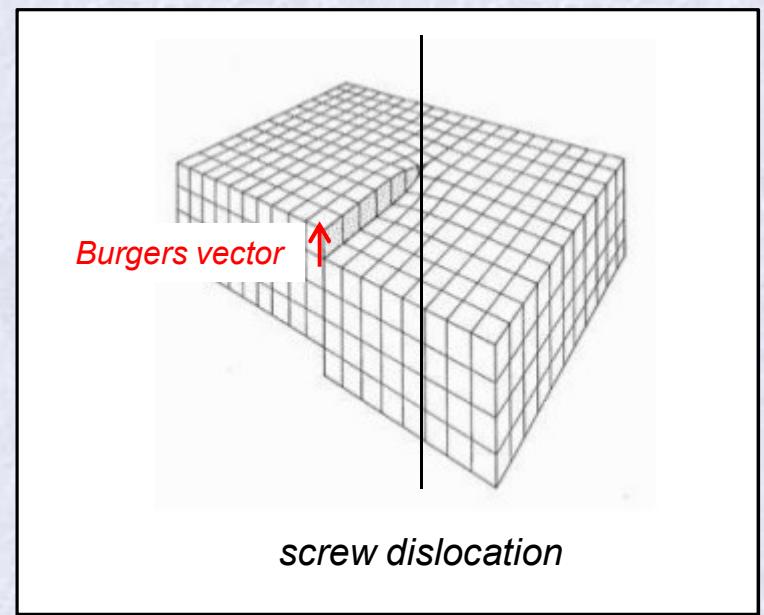
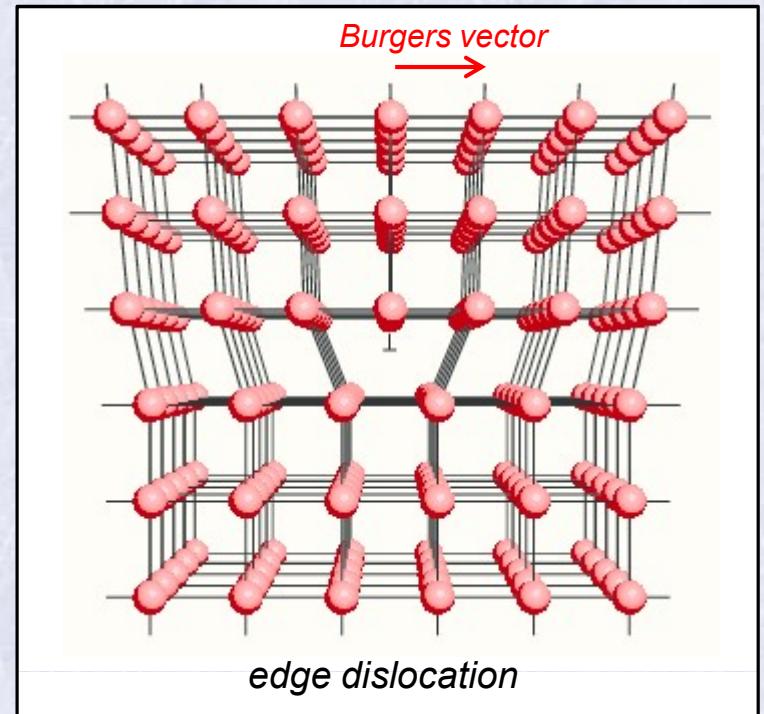
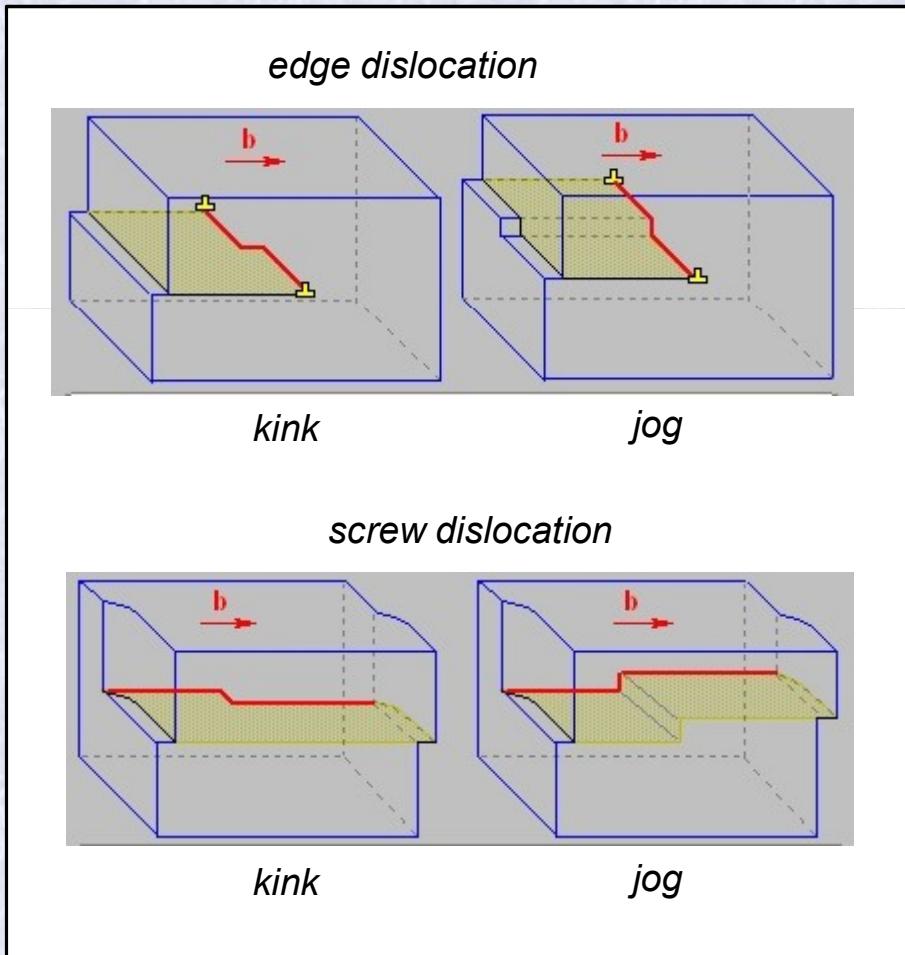
## Lattice defects in solids

- defect = any irregularity of crystalline lattice
- point defects (e.g. vacancies)



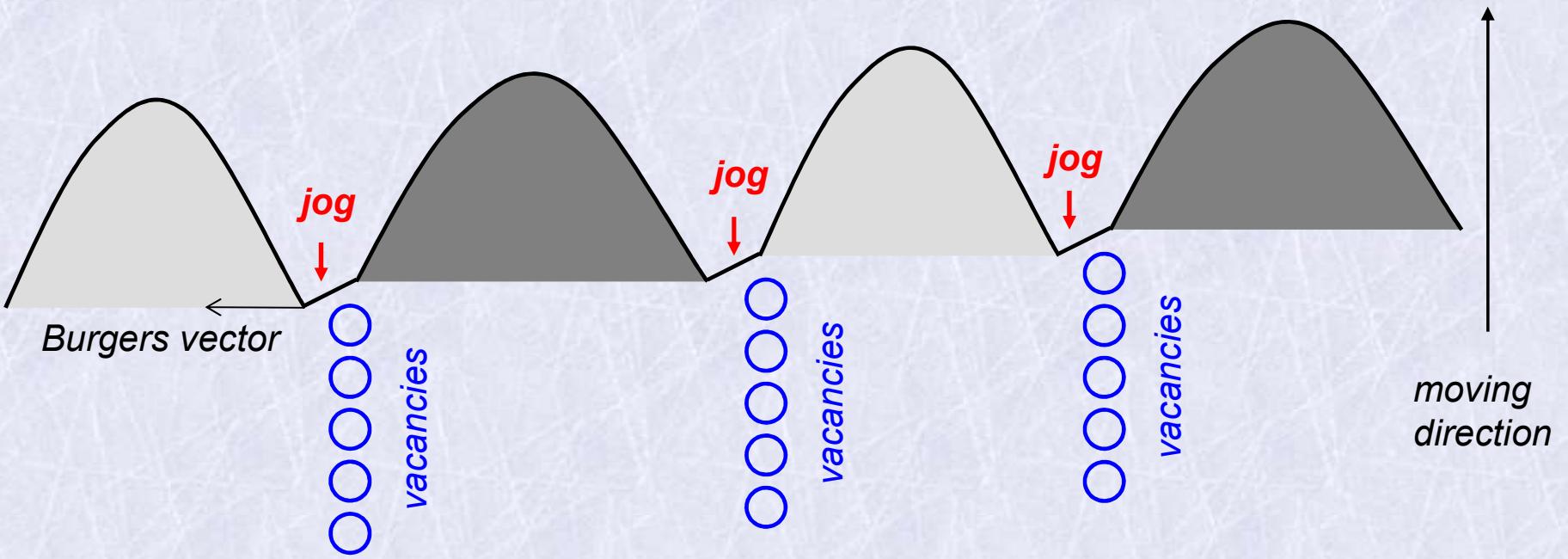
## Lattice defects in solids

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- line defects (e.g. dislocations)



## Lattice defects in solids

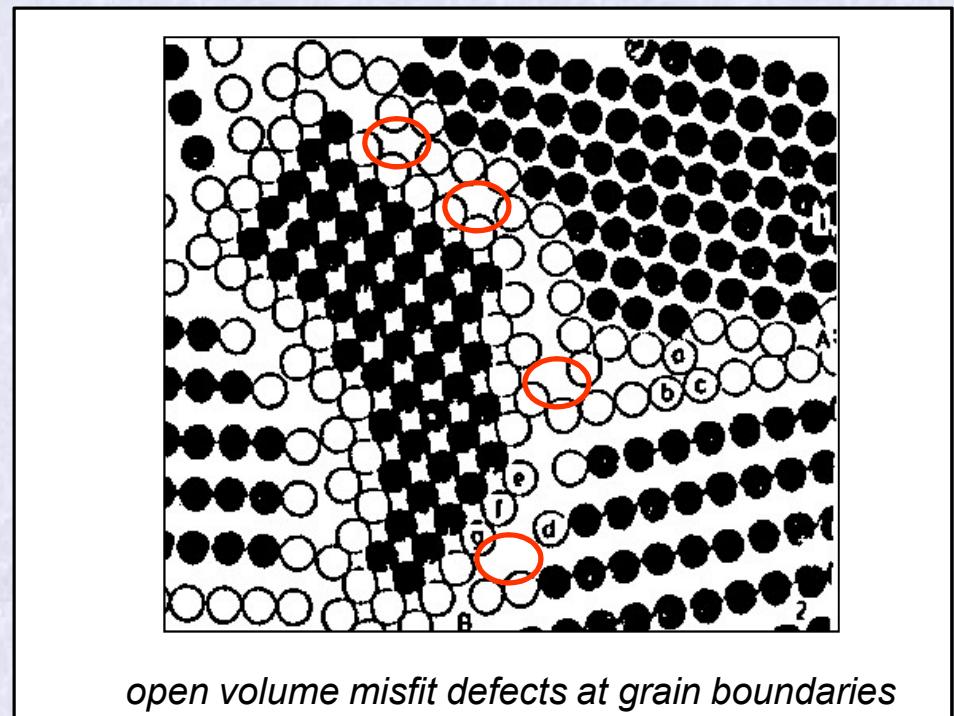
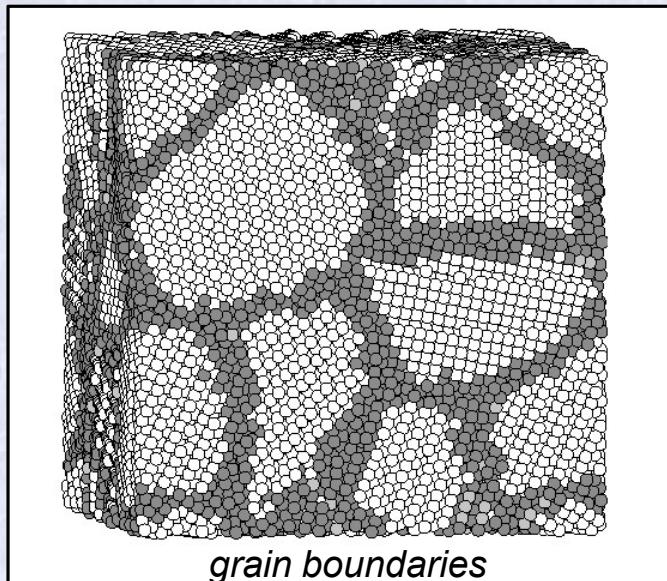
- defect = any irregularity of crystalline lattice
- line defects (e.g. dislocations)



- slip of a screw dislocation with a jogs

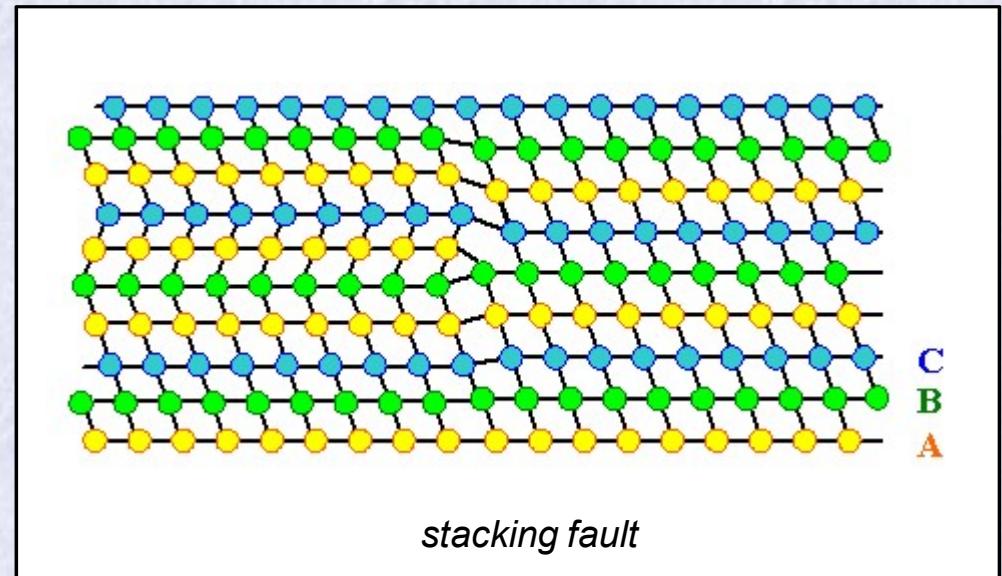
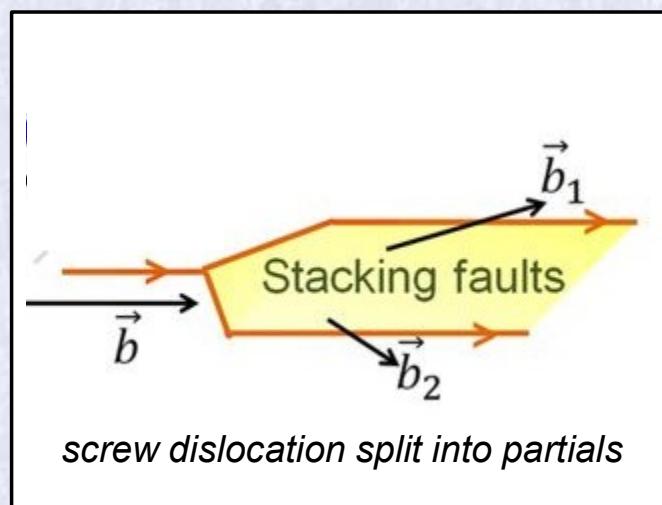
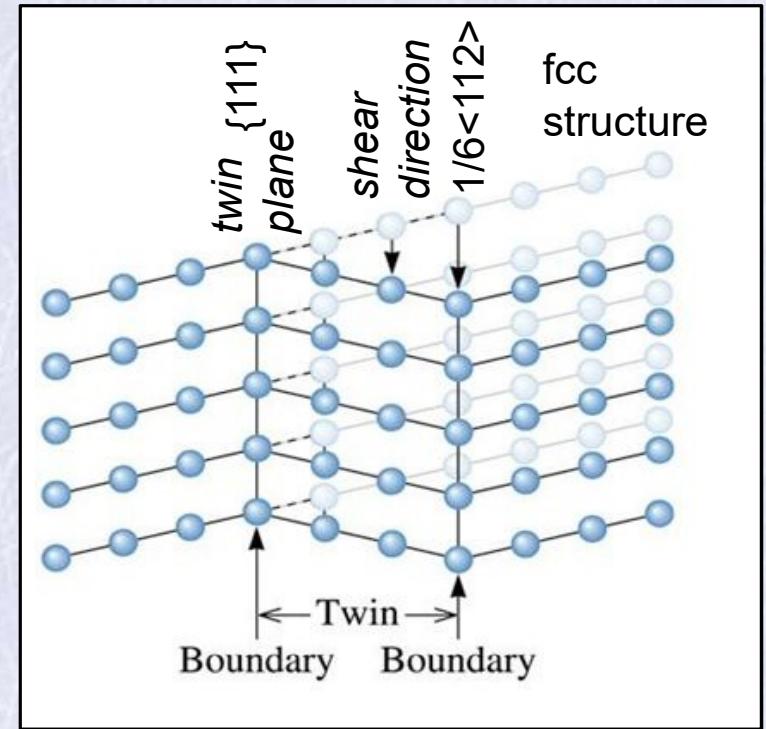
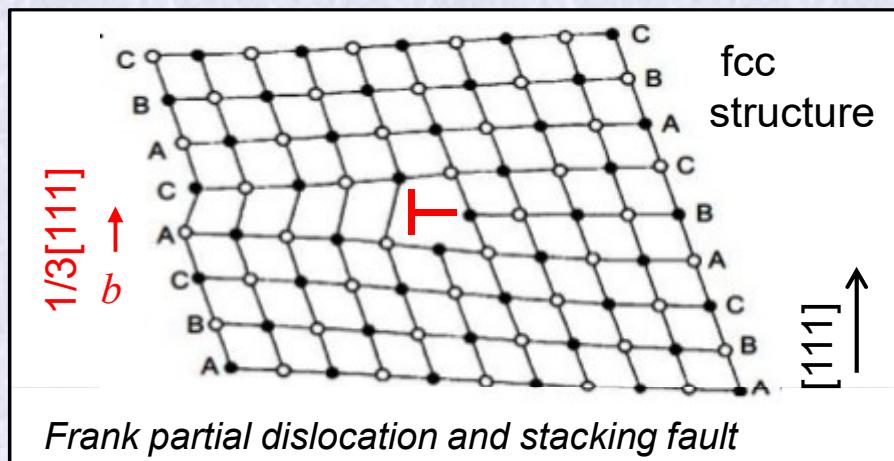
## Lattice defects in solids

- defect = any irregularity of crystalline lattice
- areal defects (e.g. grain boundaries)



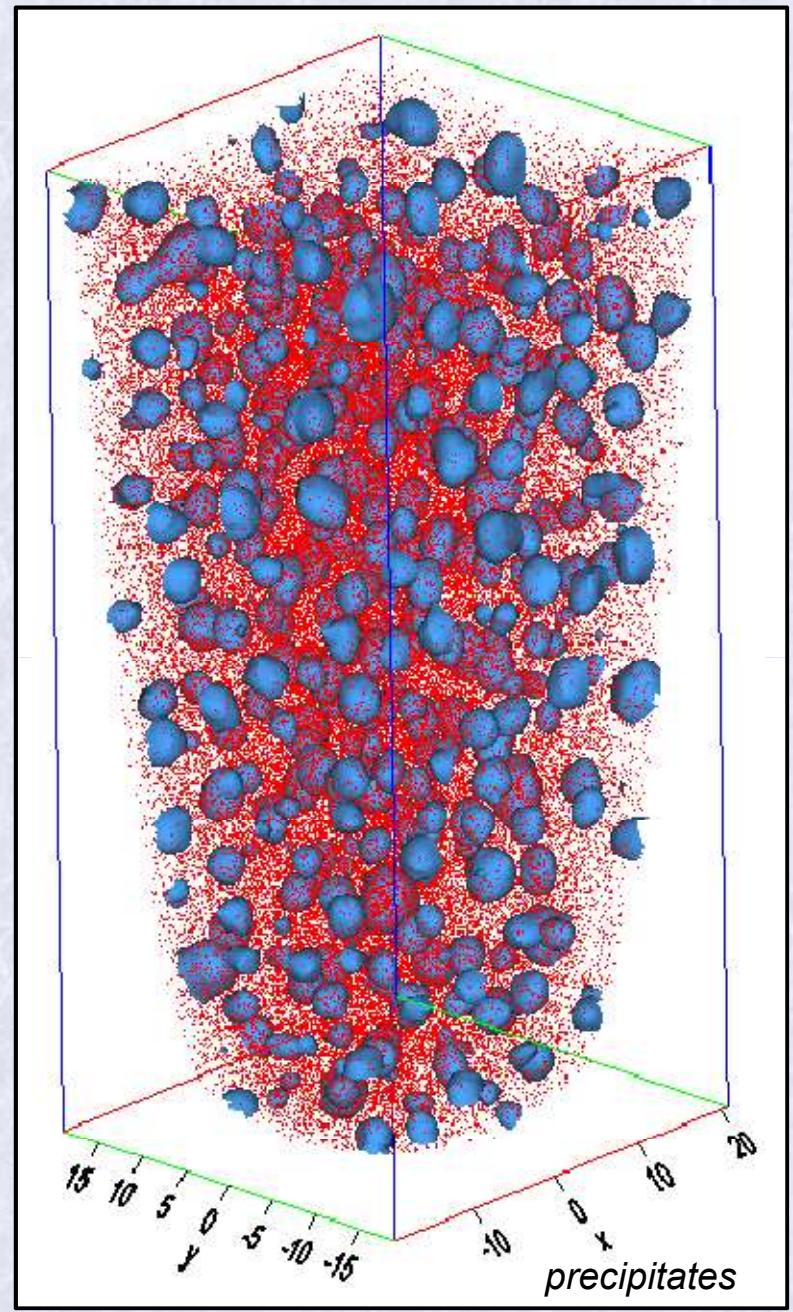
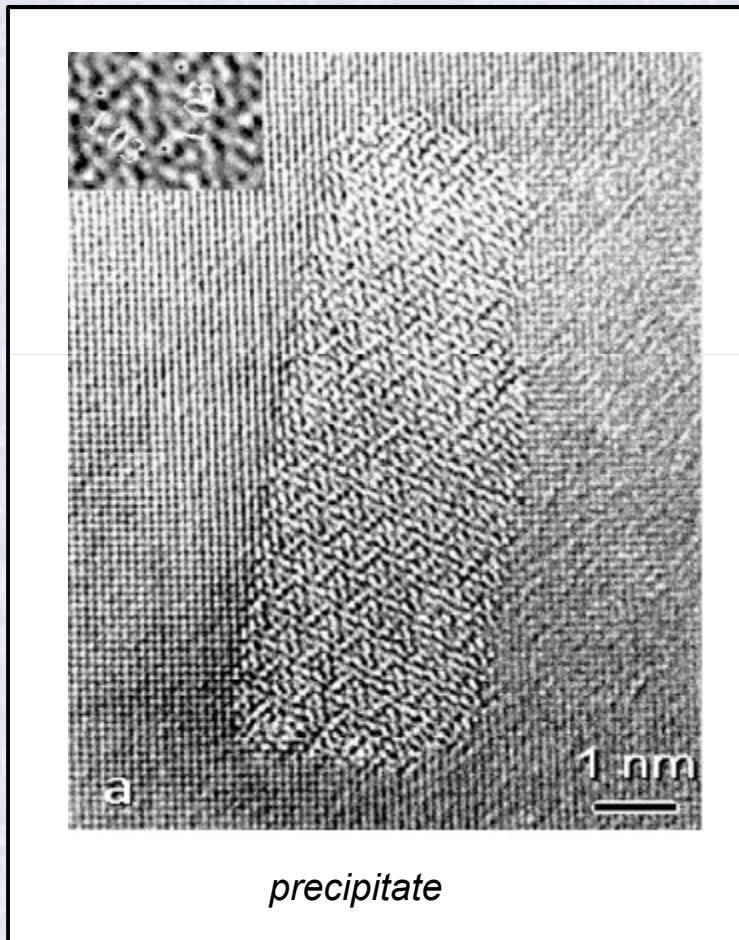
## Lattice defects in solids

- defect = any irregularity of crystalline lattice
- areal defects (e.g. grain boundaries)



## Lattice defects in solids

- defect = any irregularity of crystalline lattice
- volume defects (e.g. precipitates)



## **PAS techniques for defect studies**

- **positron lifetime (LT) spectroscopy**
  - identification of type of defects
  - determination of defect concentrations
- **coincidence Doppler broadening (CDB)**
  - local chemical environment of defects
- **variable energy positron annihilation spectroscopy (VEPAS)**
  - defect depth profile
  - positron diffusion length

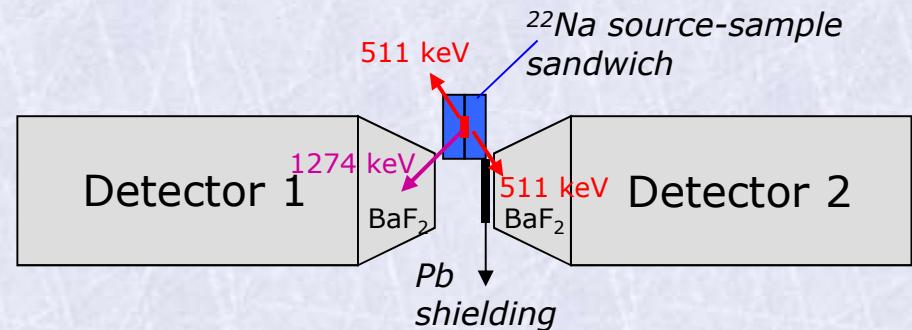
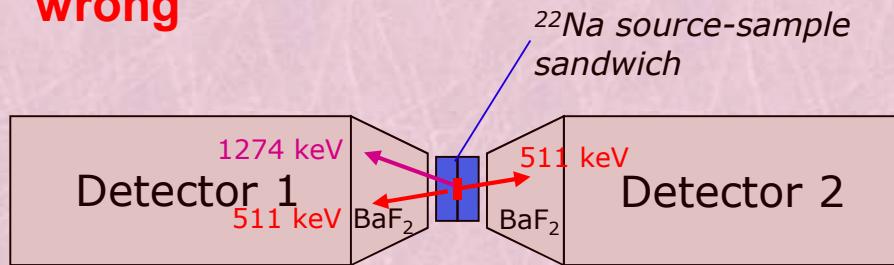
## **PAS techniques for defect studies**

- **digital spectrometers**

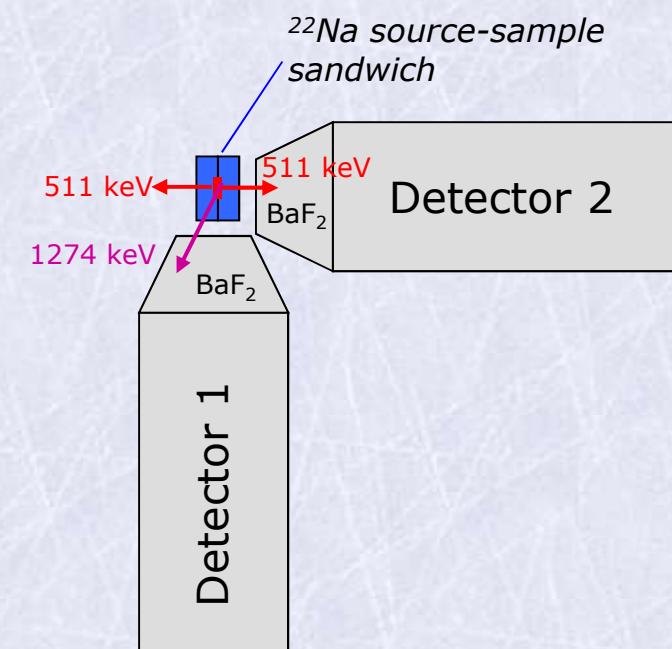
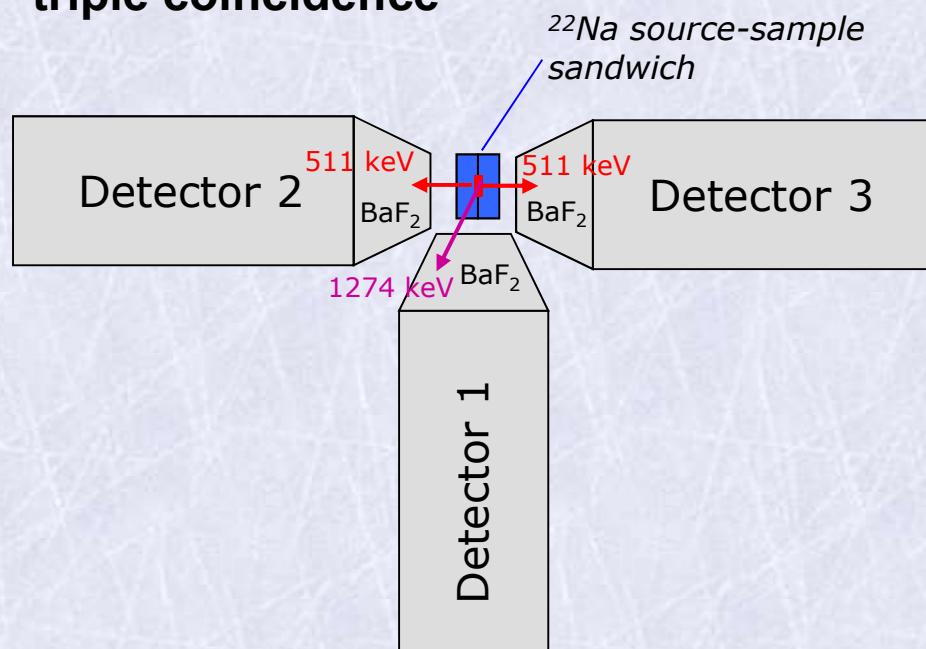
- real time sampling of detector pulses and analysis by dedicated software
- analysis can be repeated to find optimum strategy for determination of measured quantity
- perfect control over shape of sampled waveforms → excellent clarity of spectrum

# Geometry of positron lifetime spectrometer

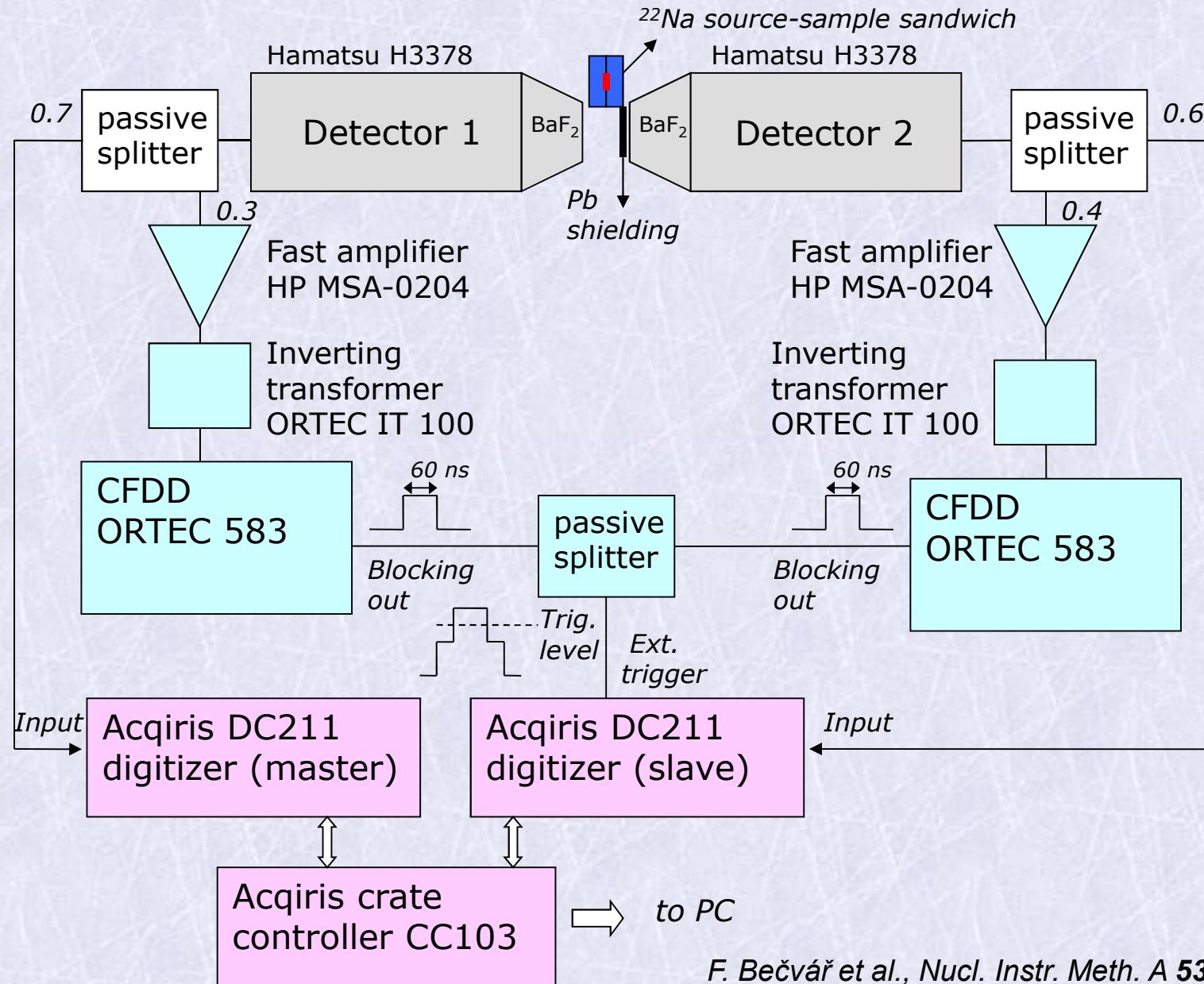
wrong



triple coincidence

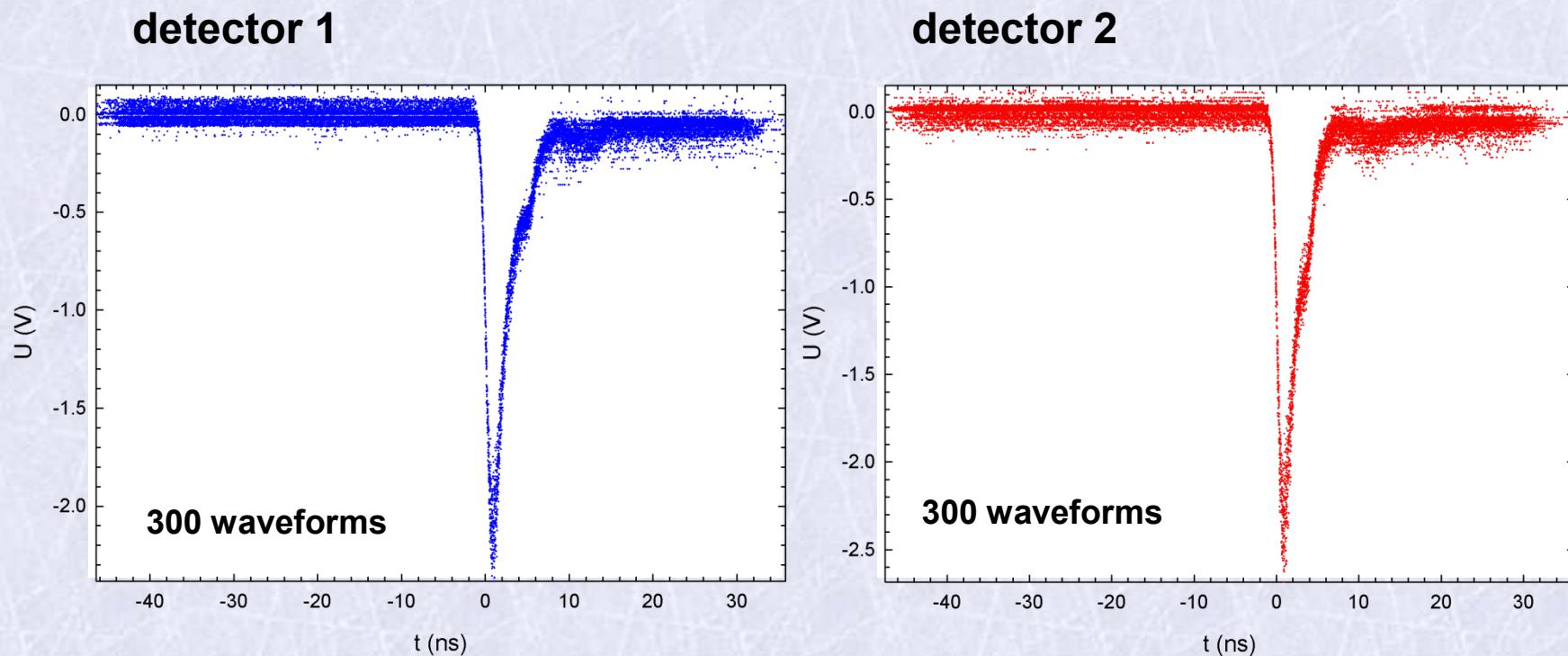


# Digital positron lifetime spectrometer



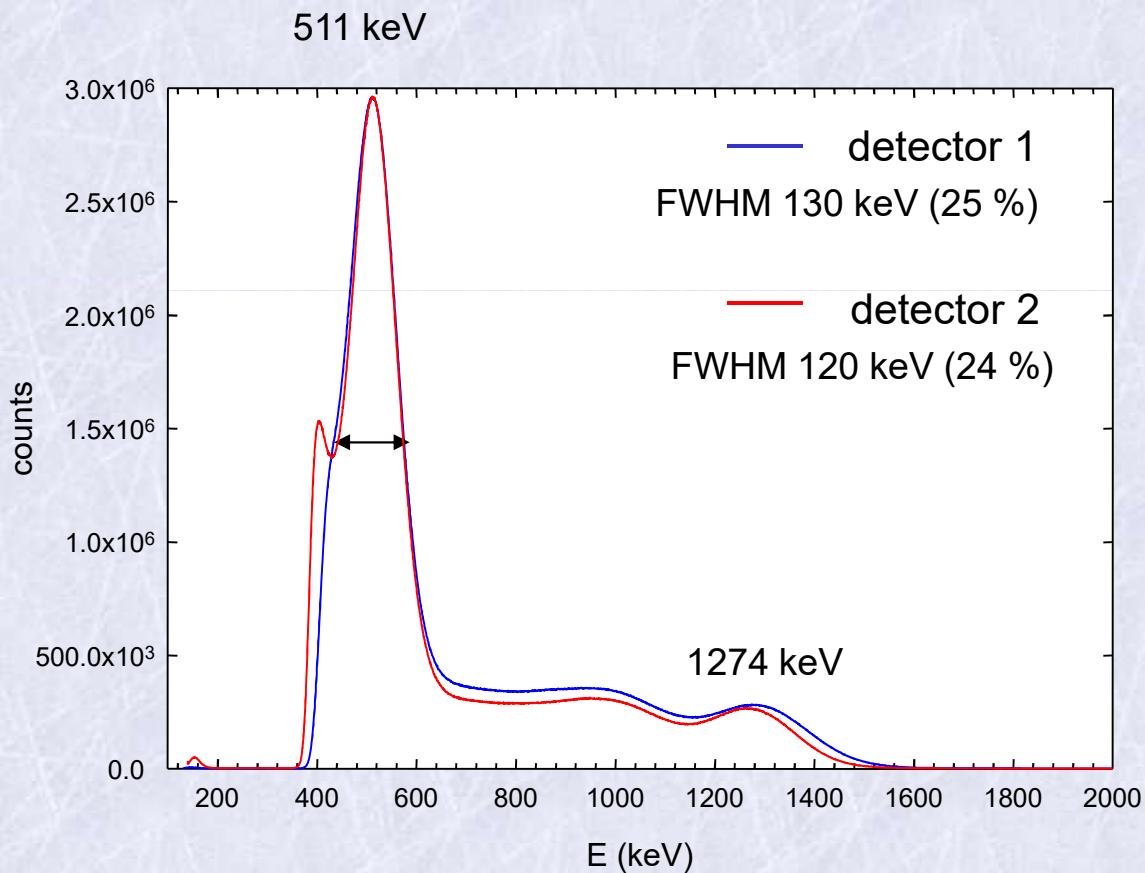
# Digital positron lifetime spectrometer

- **waveform** - single digitized detector pulse (300 points, 75 ns)
- normalized waveforms



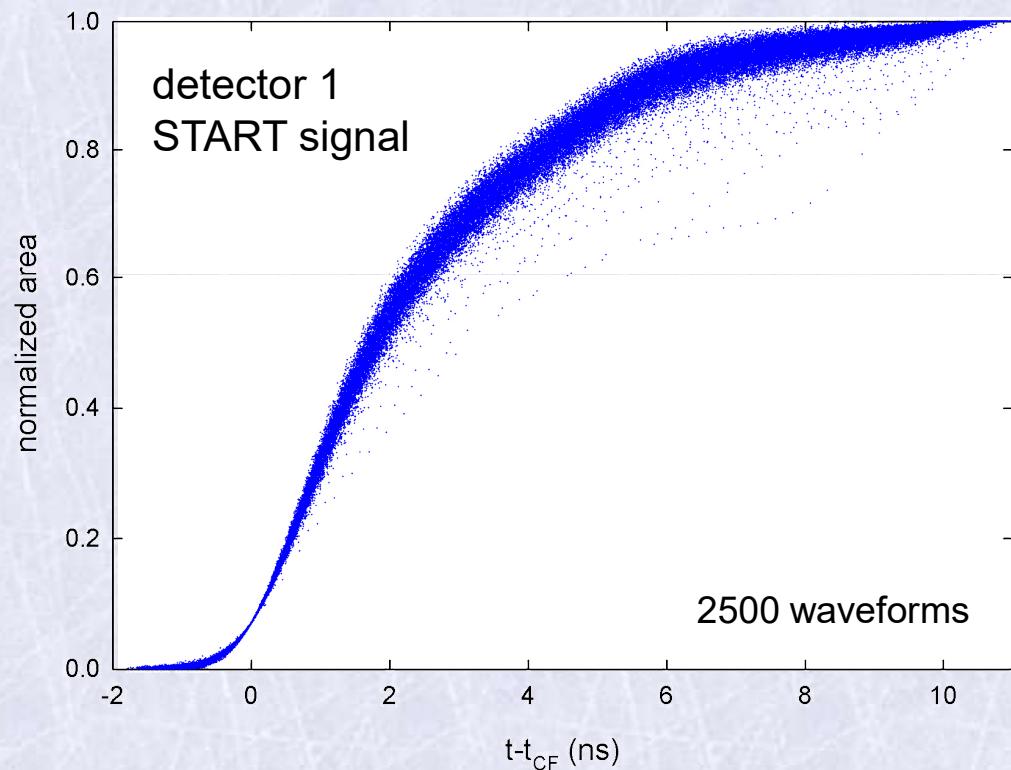
# Digital positron lifetime spectrometer

- $\gamma$ -ray energy spectrum obtained by integration of waveforms



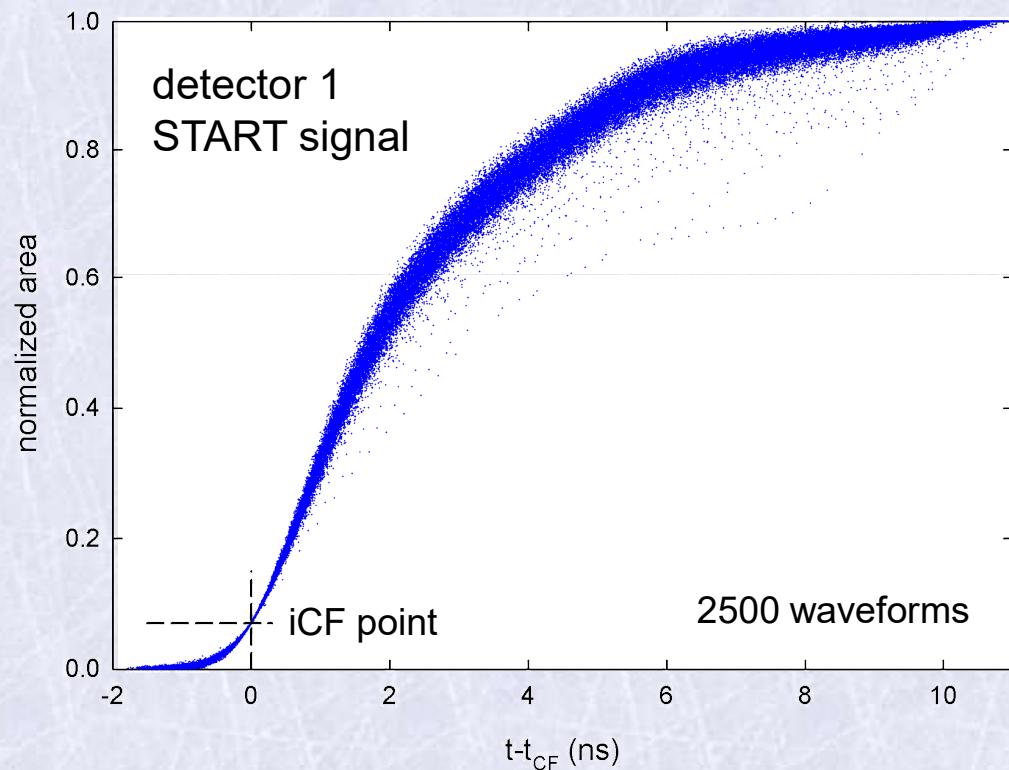
# Digital positron lifetime spectrometer

- *integral* constant fraction timing iCF



# Digital positron lifetime spectrometer

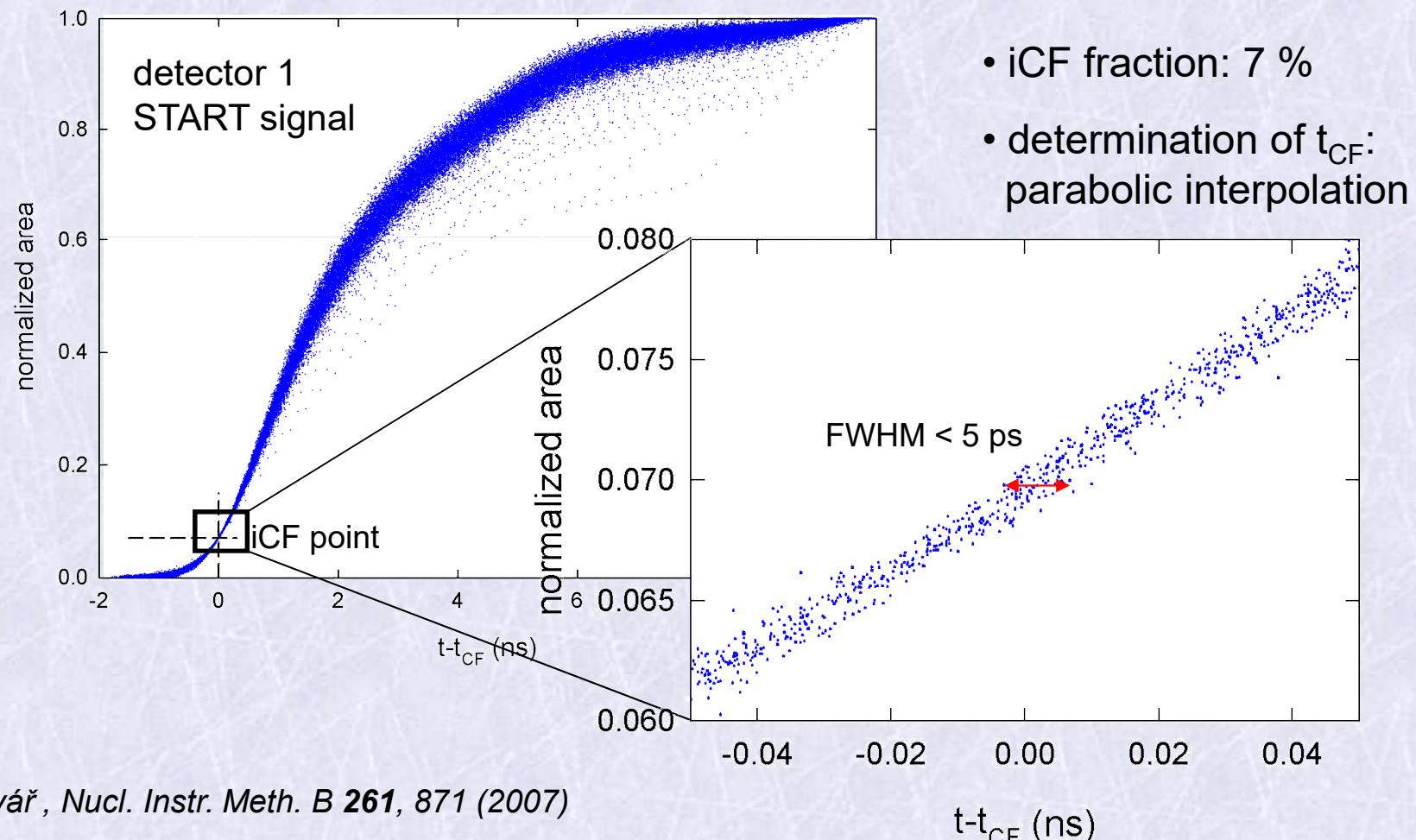
- *integral* constant fraction timing iCF



- iCF fraction: 7 %
- determination of  $t_{CF}$ : parabolic interpolation

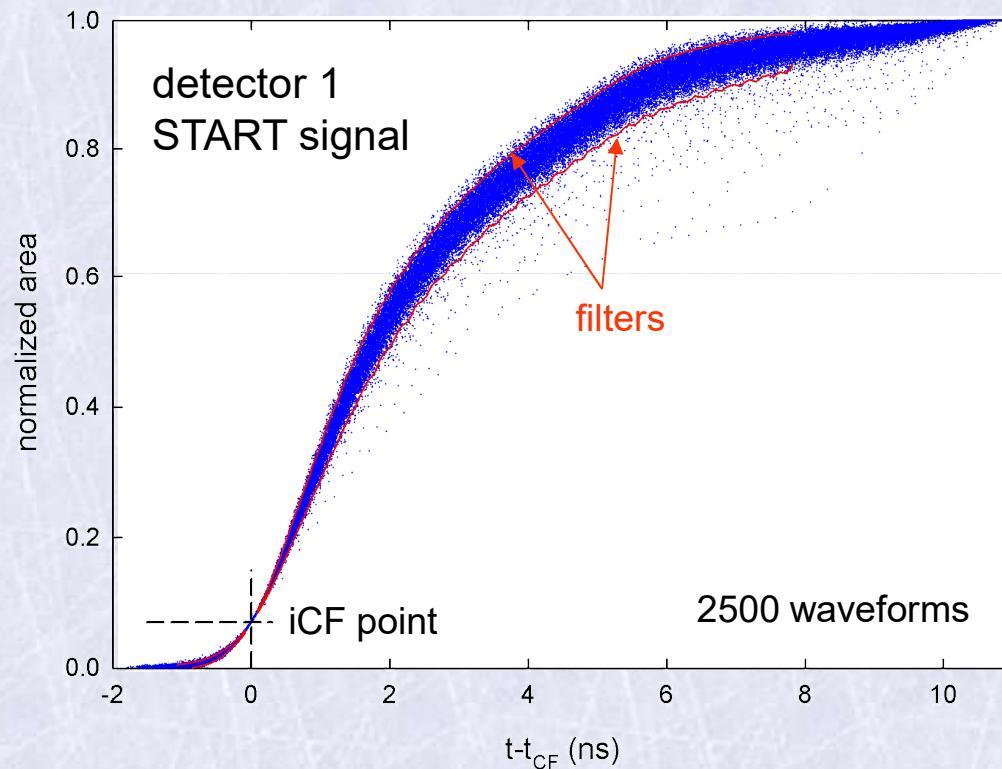
# Digital positron lifetime spectrometer

- integral constant fraction timing iCF



# Digital positron lifetime spectrometer

- *integral* constant fraction timing iCF
- shape of pulses controlled by **digital filters** – majorizing and minorizing function

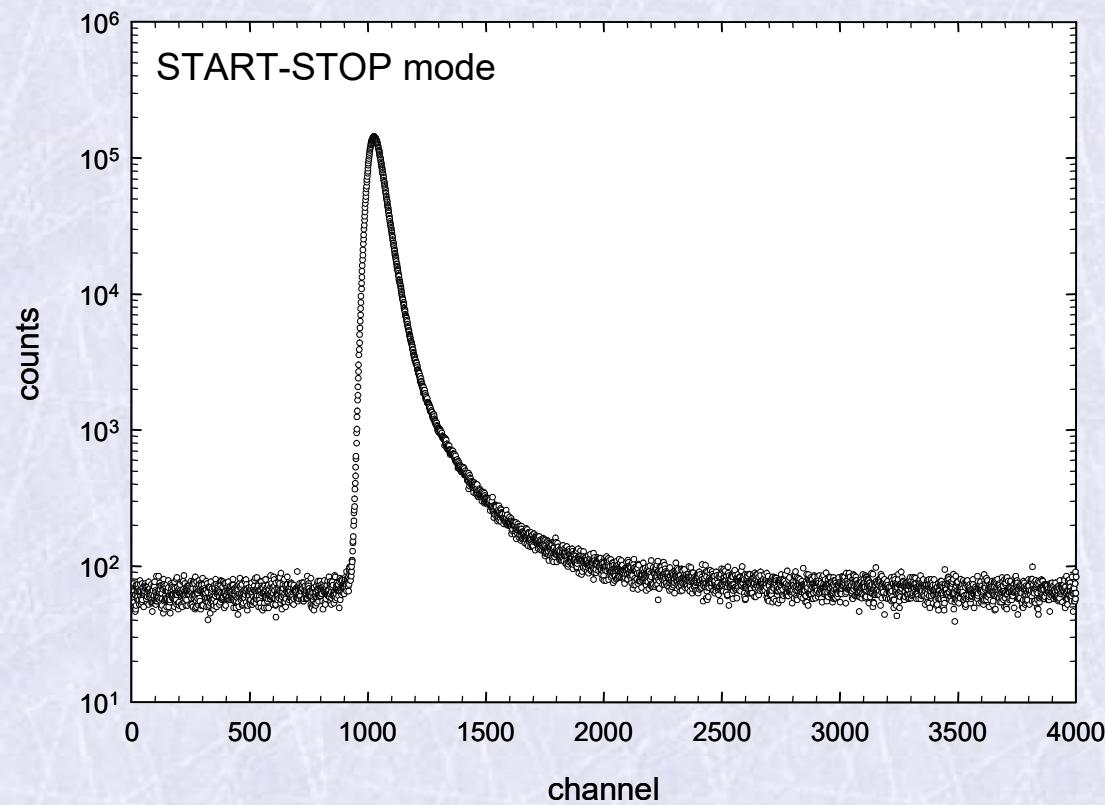


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# Digital positron lifetime spectrometer

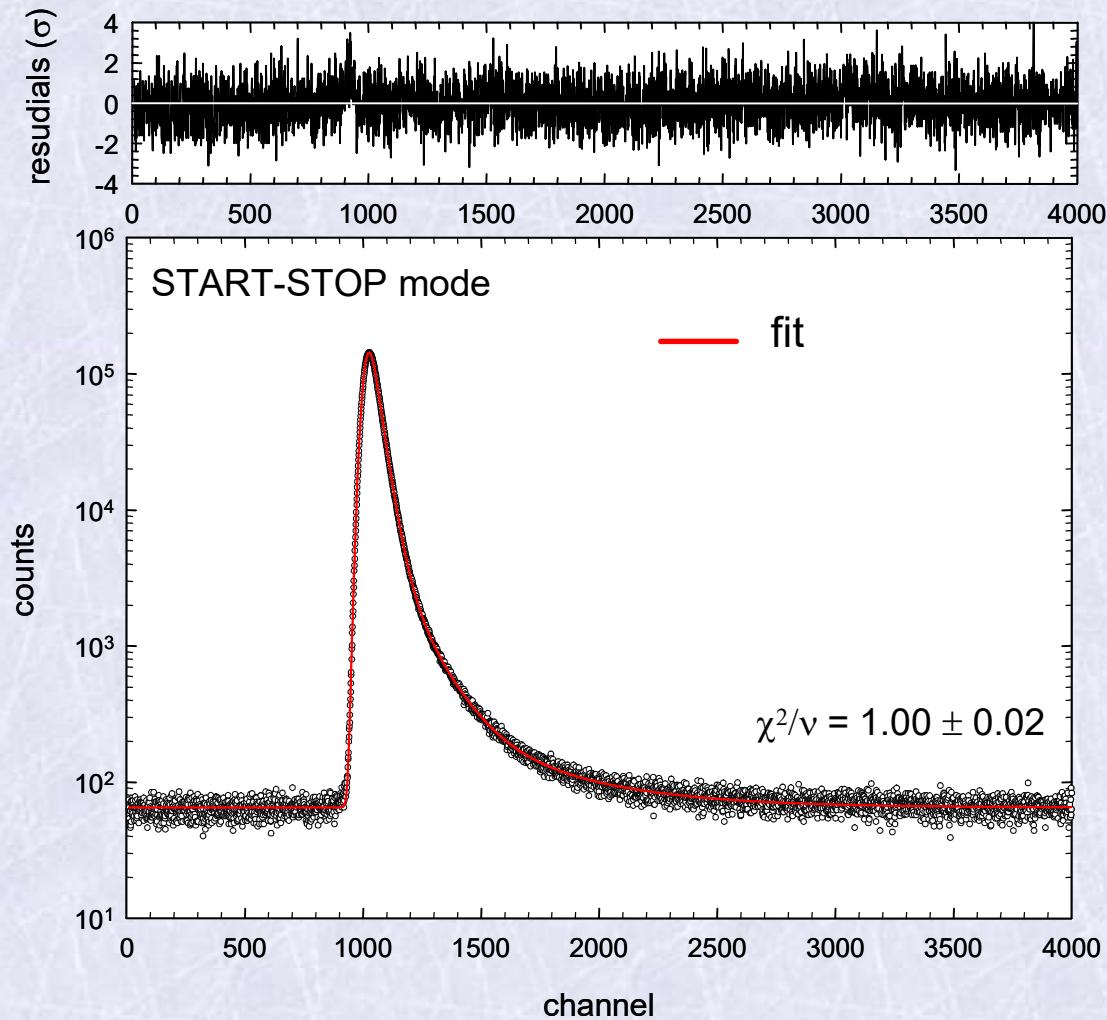
- standard source (1.2 MBq),  $\alpha$ -Fe reference specimen

- statistics:  $8 \times 10^6$



# Digital positron lifetime spectrometer

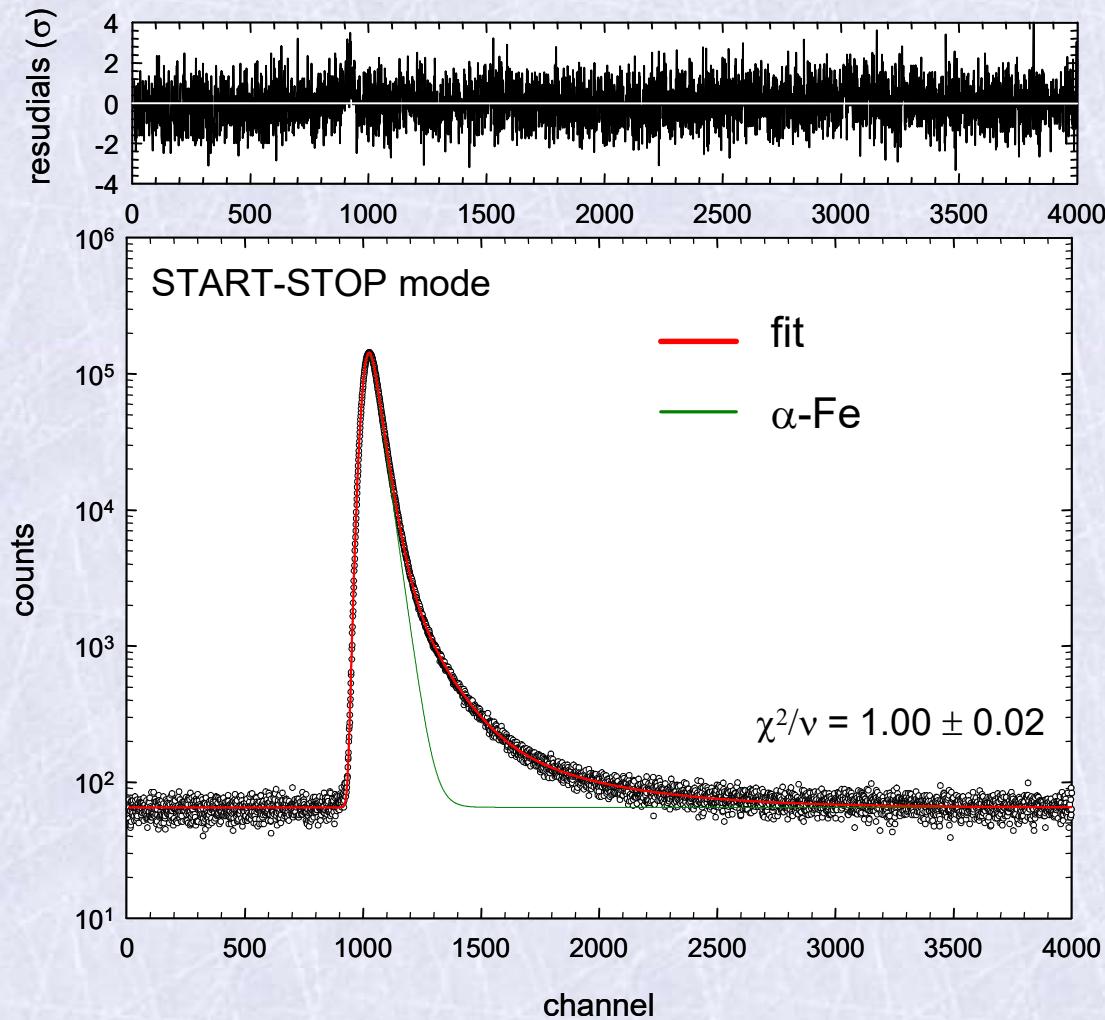
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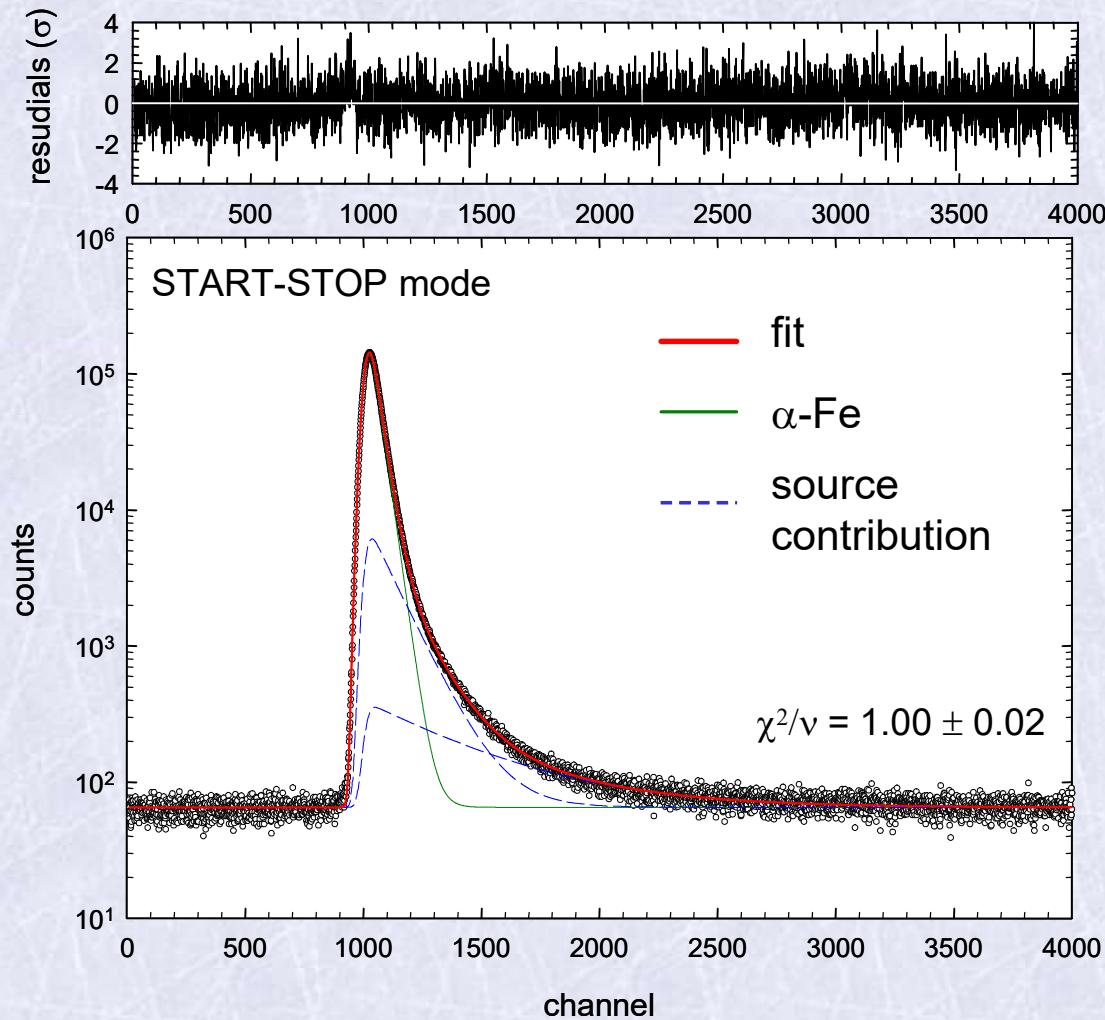
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- standard source (1.2 MBq),  $\alpha$ -Fe reference specimen



- statistics:  $8 \times 10^6$
- $\alpha$ -Fe:  $\tau = (107.0 \pm 0.3)$  ps
- **time resolution:**  
**143 ps (FWHM)**
- resolution function:  
two Gaussians

## Digital positron lifetime spectrometer

- standard source (1.2 MBq),  $\alpha$ -Fe reference specimen
- START-STOP mode
- count rate:  $940 \text{ s}^{-1}$
- accumulated coincidences:  $200 \times 10^6$  (2.5 day)

---

  - waveforms outside energy windows:  $156 \times 10^6$  (77.9 %)
  - waveforms rejected by digital filters:  $34 \times 10^6$  (17.1 %)
  - waveforms rejected due to too noisy baseline:  $1.6 \times 10^6$  (0.8 %)

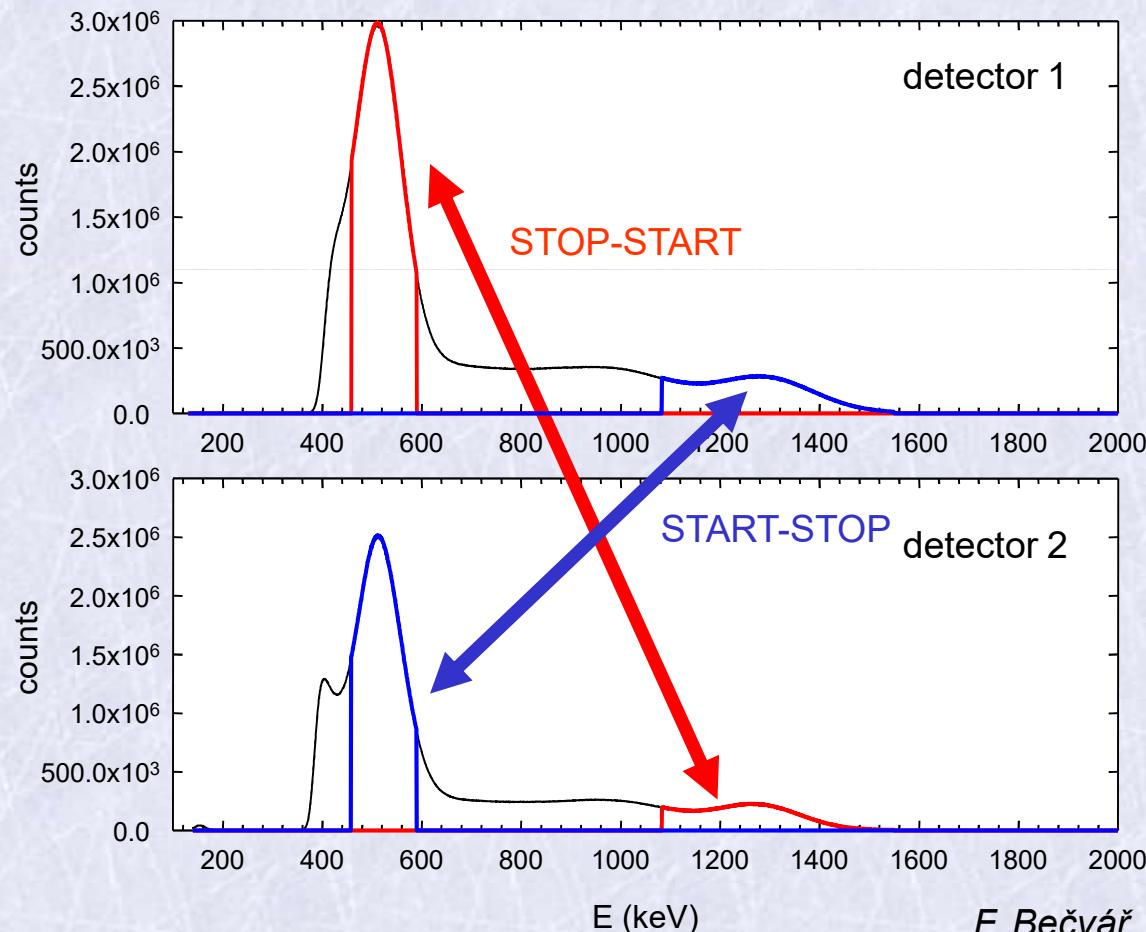
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**accepted waveforms:  $8.4 \times 10^6$  (4.2 %)**

(effective coincidence count rate:  $40 \text{ s}^{-1}$ )

# Digital positron lifetime spectrometer

- standard source (1.2 MBq),  $\alpha$ -Fe reference specimen
- **energy windows:** START: (1080-1550) keV, STOP (460-590)
- **double count rate at no cost**



## START-STOP mode:

detector 1: START  
detector 2: STOP

## STOP-START mode:

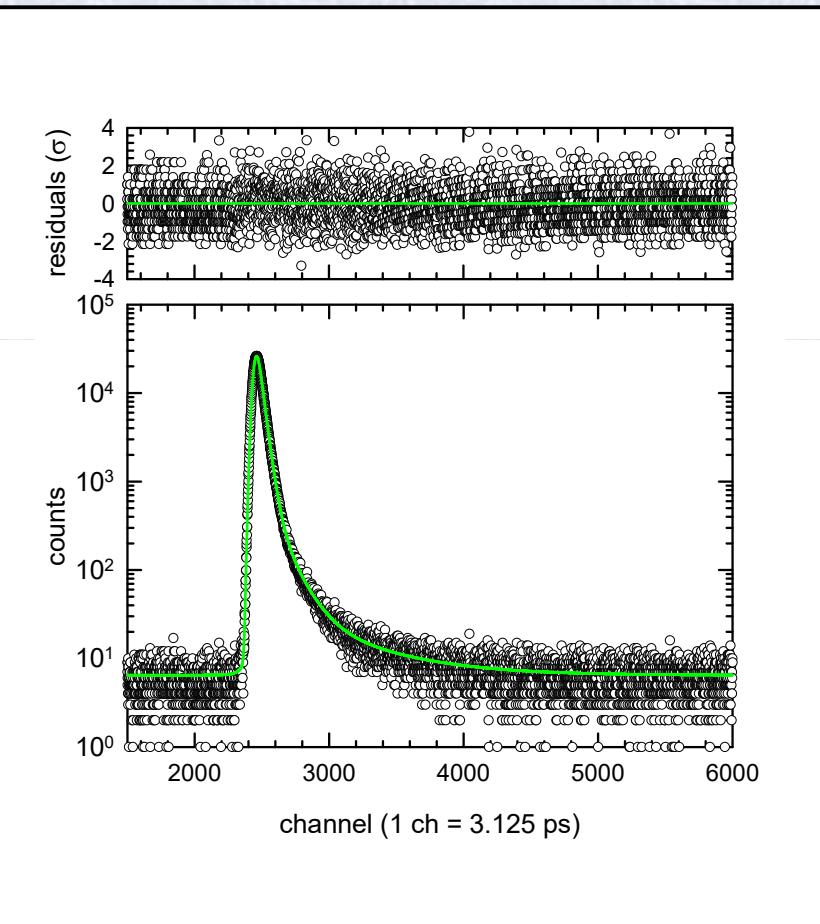
detector 1: STOP  
detector 2: START

# Digital positron lifetime spectrometer

## START-STOP mode:

detector 1: START

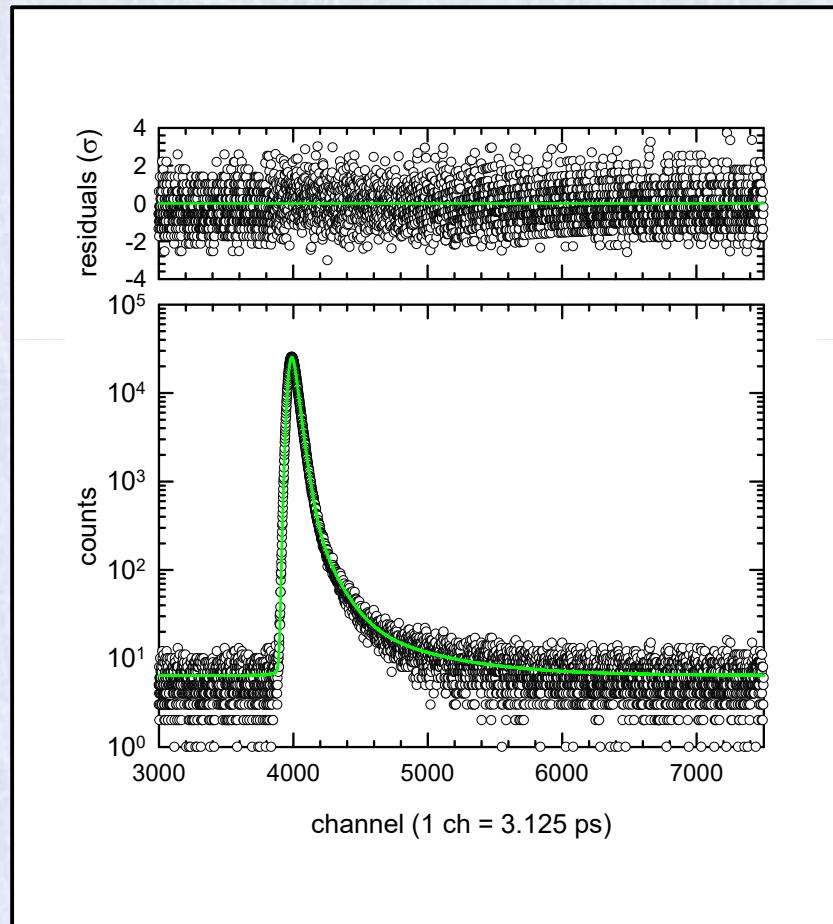
detector 2: STOP



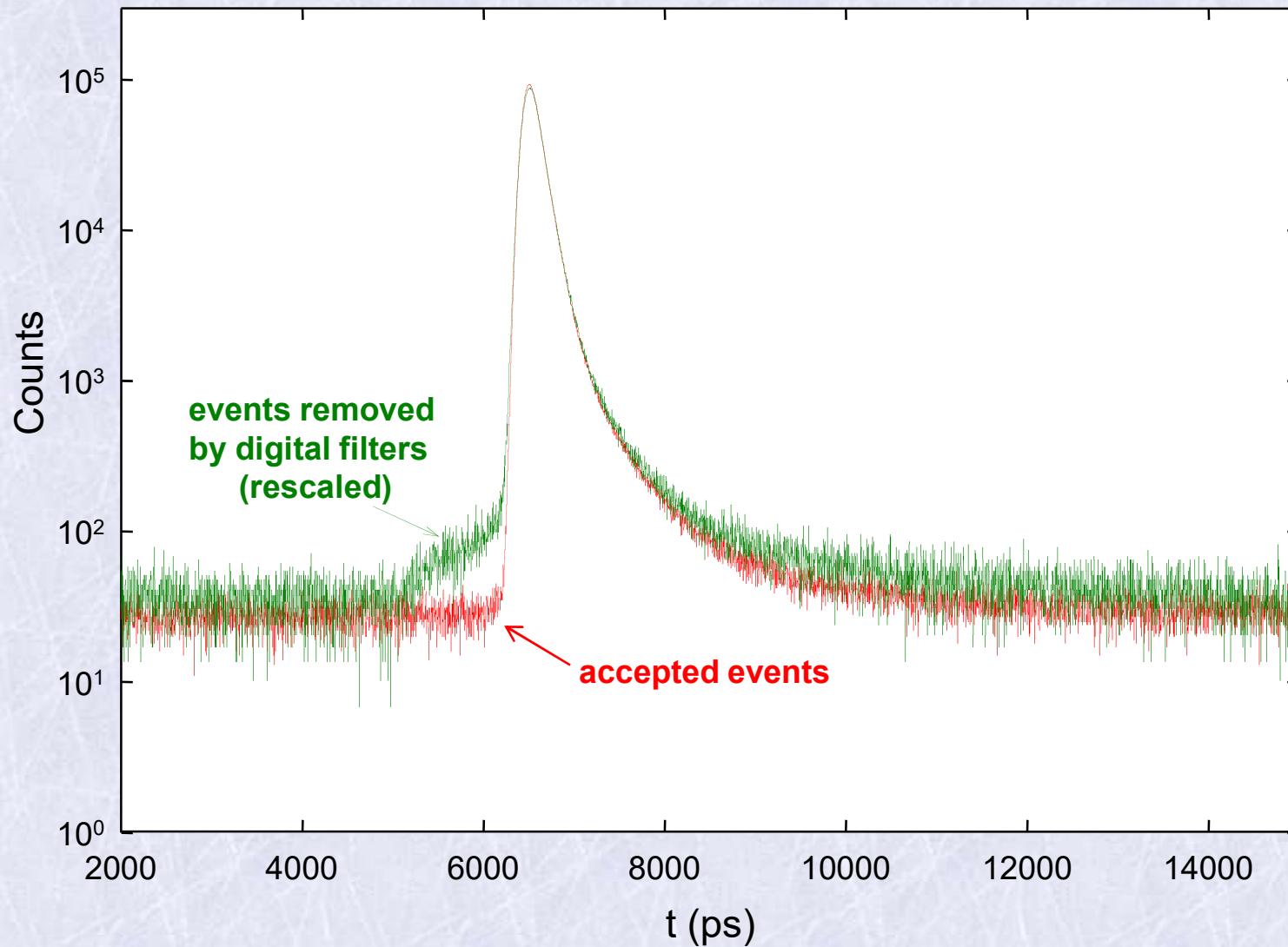
## STOP-START mode:

detector 1: STOP

detector 2: START



# Digital positron lifetime spectrometer



## LT spectroscopy

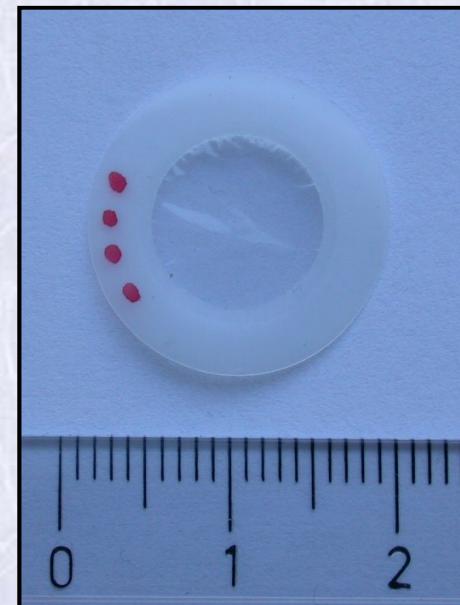
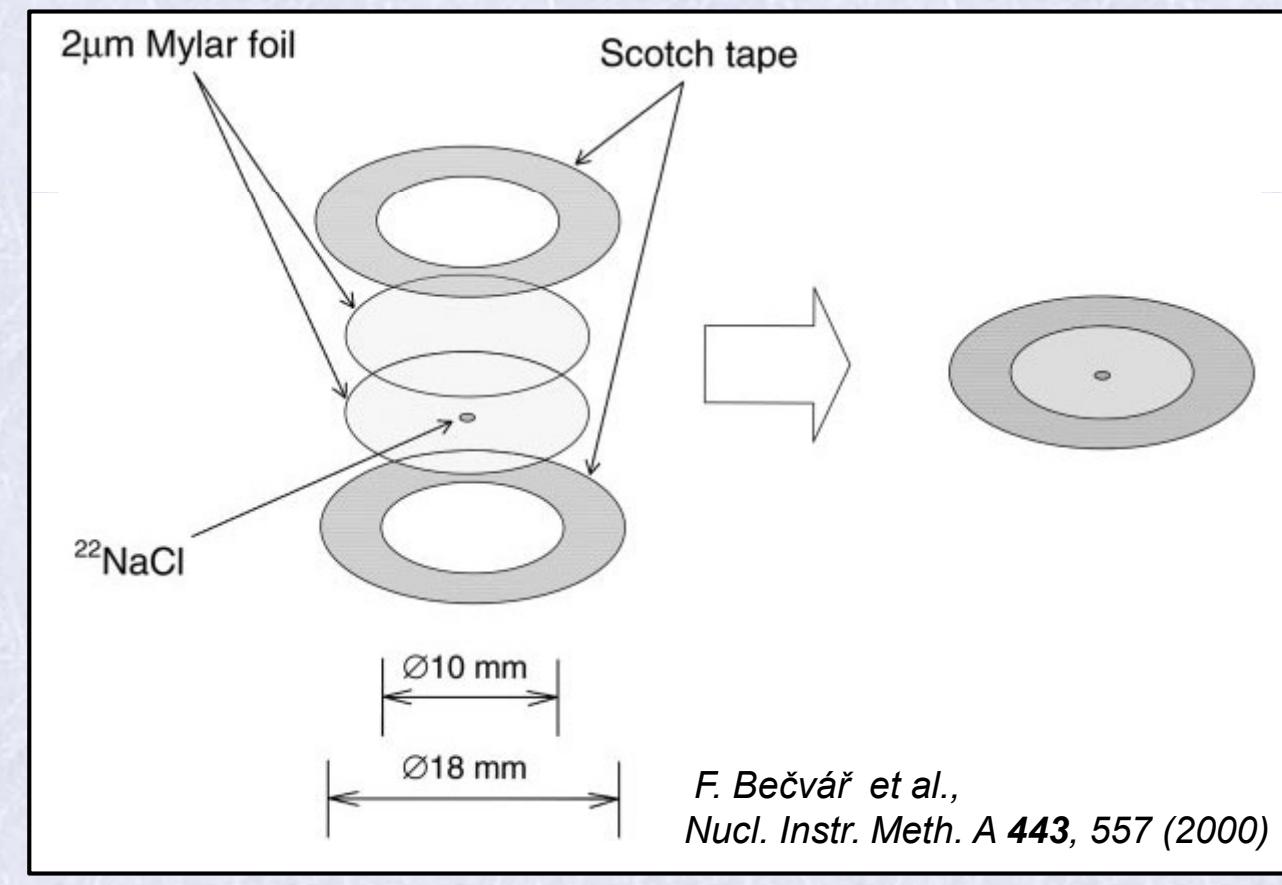
- what is necessary to know for meaningful fitting of LT spectra
  - time calibration      *F. Bečvář et al., Mater. Sci. Forum 363-365, 695 (2001)*
  - source contribution
  - resolution function
- } measurement of well defined reference sample

## Source contribution

- positron source ( $1\text{-}3 \mu\text{l}$ )  $^{22}\text{NaCl}$  ( $1\text{-}2 \text{ MBq}$ )
  - $^{22}\text{NaCl}$  deposited on  $2 \mu\text{m}$  mylar foil:  $\tau_{s1} = 368(2) \text{ ps}$ ,
  - $^{22}\text{NaCl}$  deposited on  $7.6 \mu\text{m}$  kapton foil:  $\tau_{s1} = 403(1) \text{ ps}$
  - $^{22}\text{NaCl}$  deposited on  $5 \mu\text{m}$  Ti foil:  $\tau_{s1} = 380(5) \text{ ps}$ ,  $\tau_{s2} = 174(4) \text{ ps}$

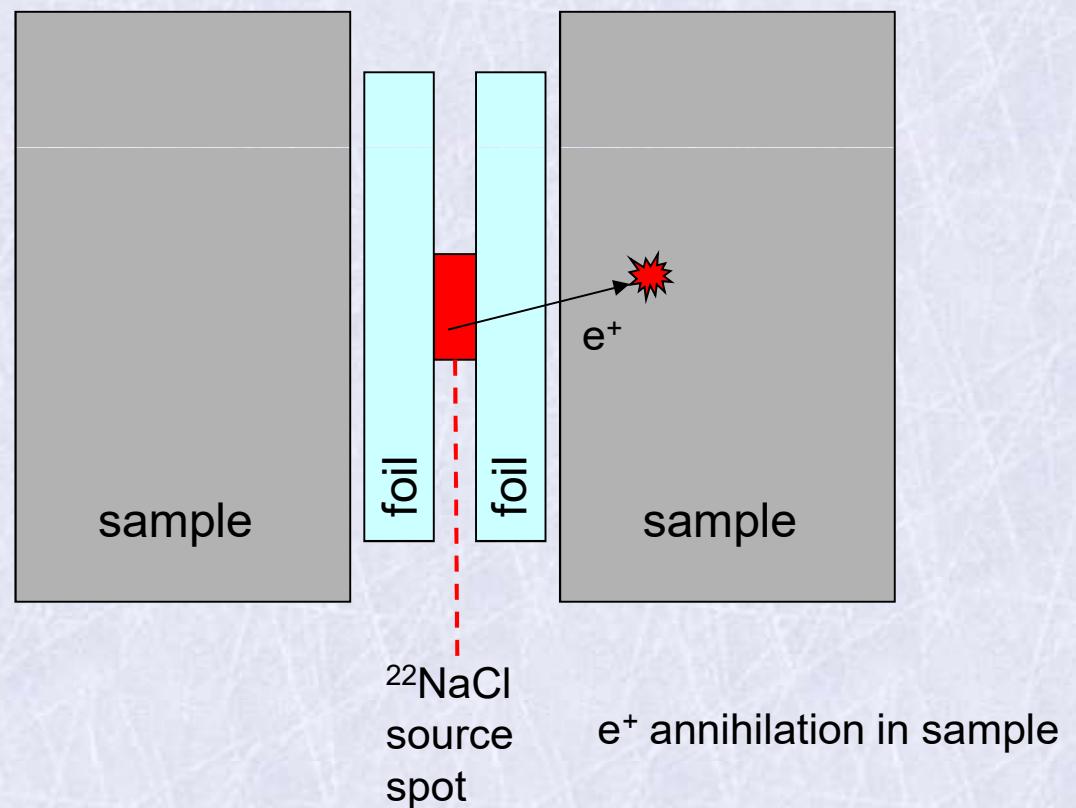
$e^+$  annihilation  
↓

Ps annihilation  
↓  
 $\tau_{s2, p-\text{Ps}} = 125 \text{ ps}$ ,  
 $\tau_{s2, o-\text{Ps}} = 1.5(3) \text{ ns}$ ,



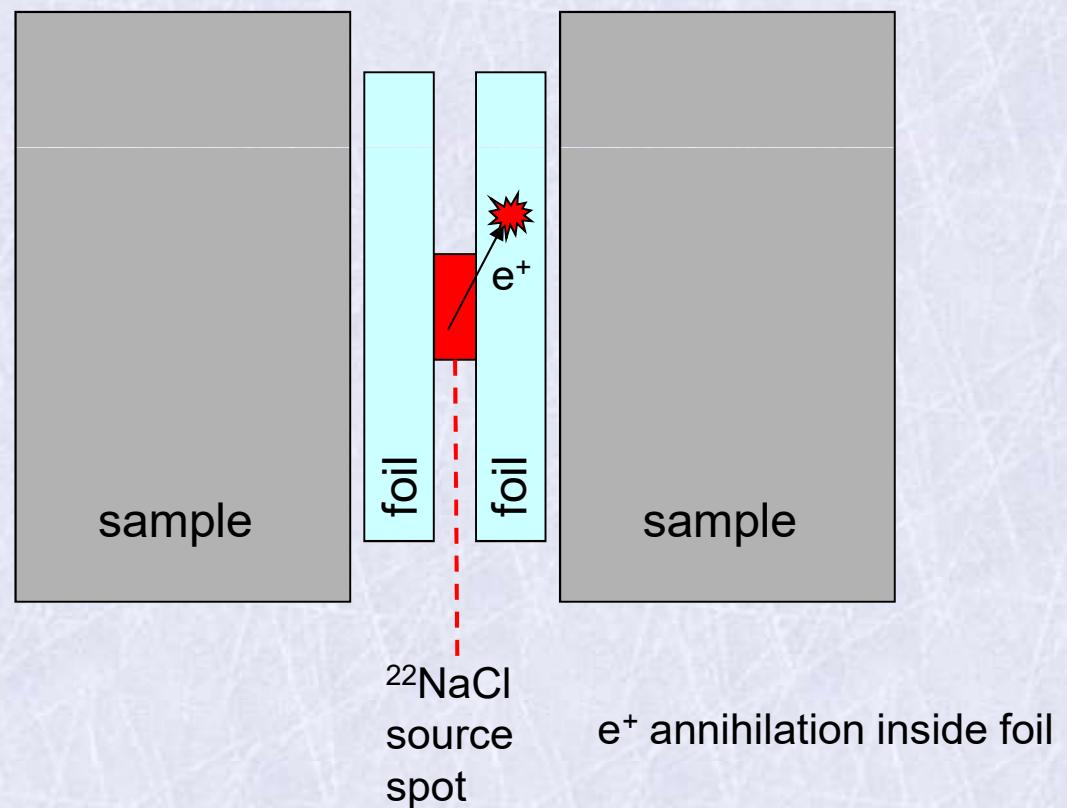
## Source contribution

- intensity of source contribution



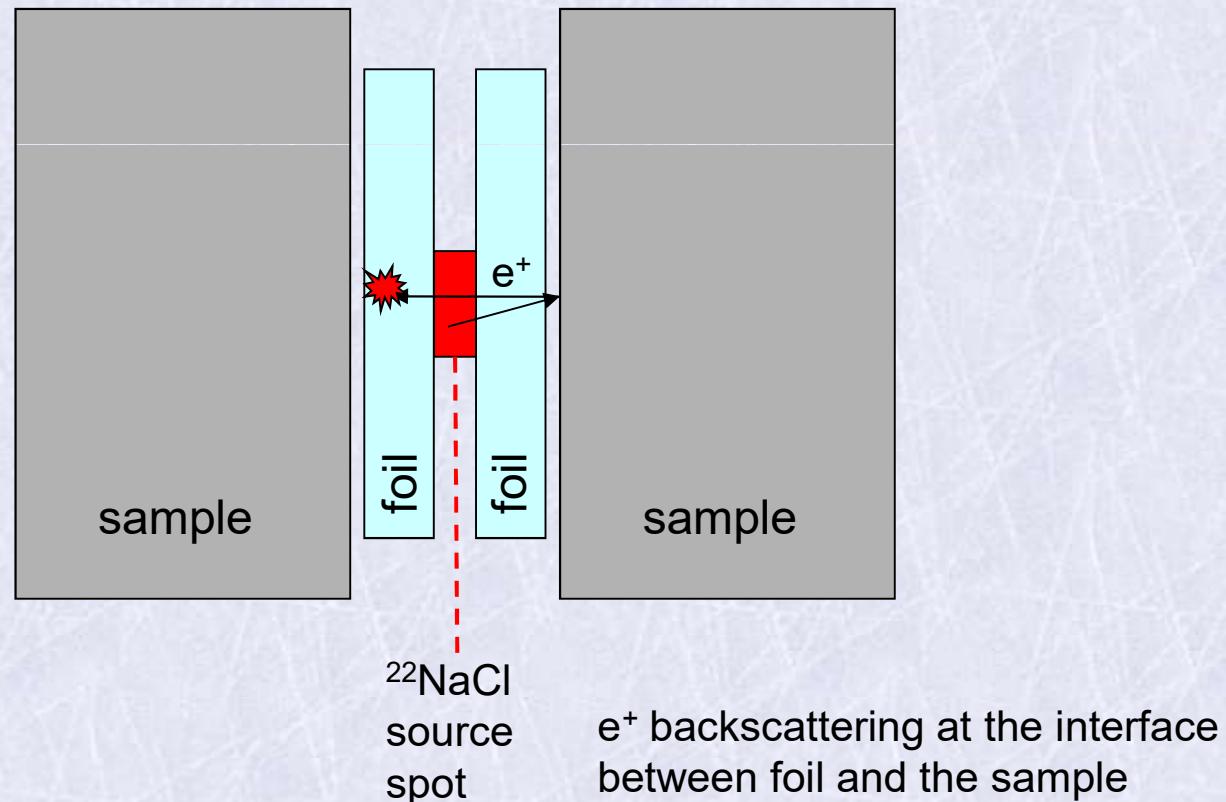
## Source contribution

- intensity of source contribution



## Source contribution

- positron reflection on the interface between materials with various Z
- positron reflectance increases with Z
- This makes intensity of the source contribution increasing with Z of the sample

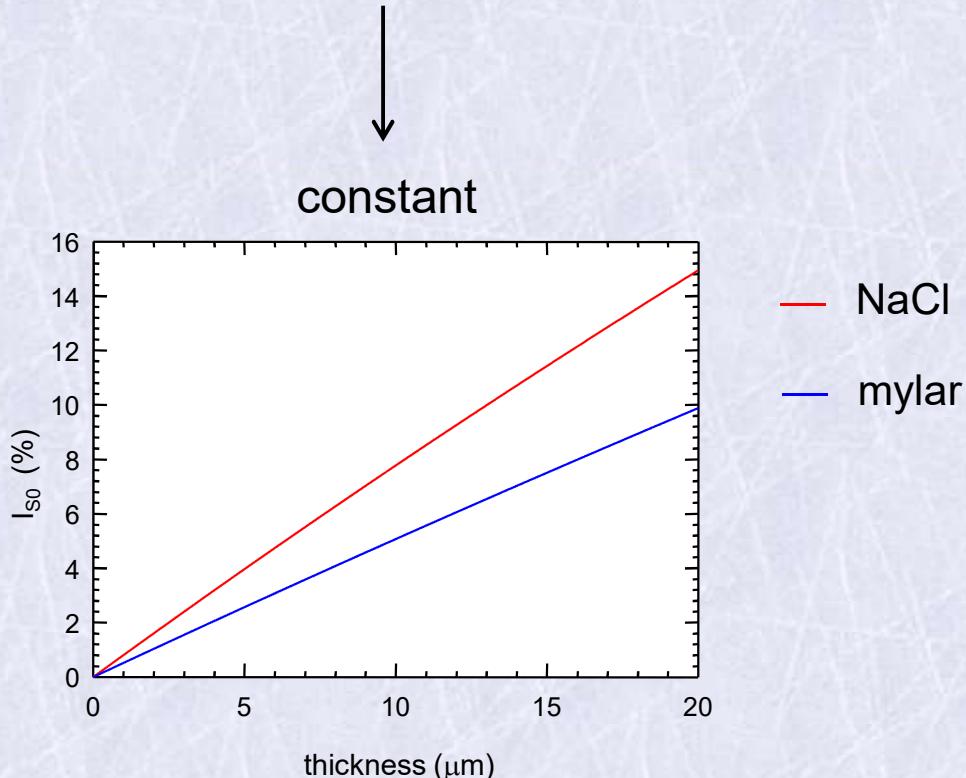
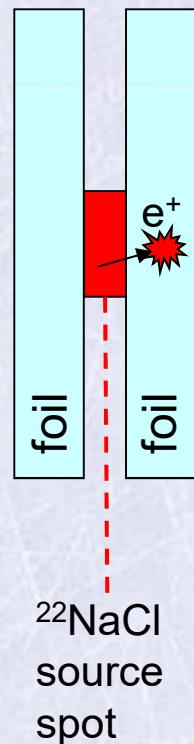


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- Intensity of the source contribution:  $I_S = I_{S0} + I(Z)$

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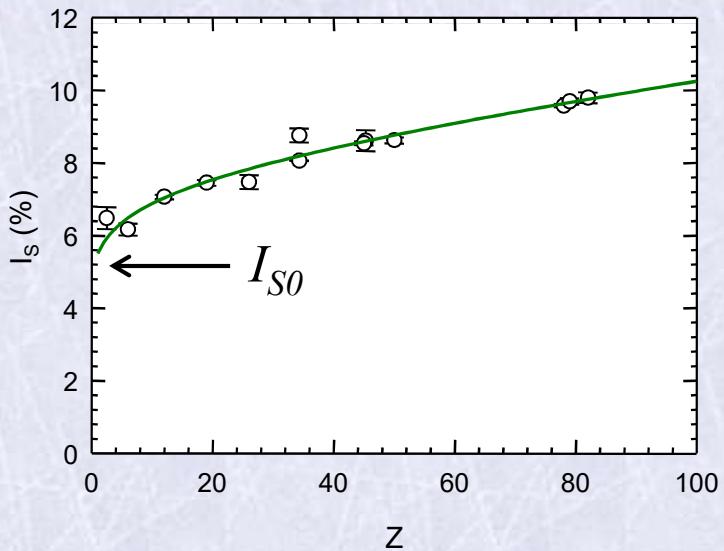


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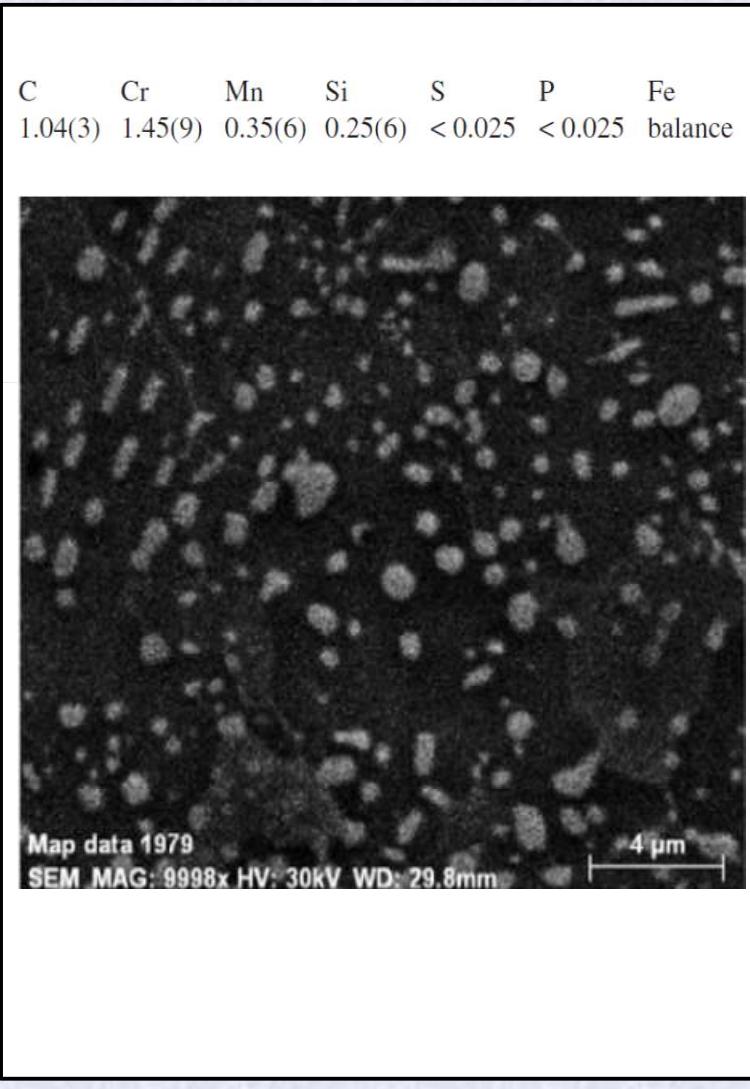
$$I(Z) = a \ln(Z + 1) + bZ$$

$$a = 0.70(1)$$
$$b = 0.020(2)$$



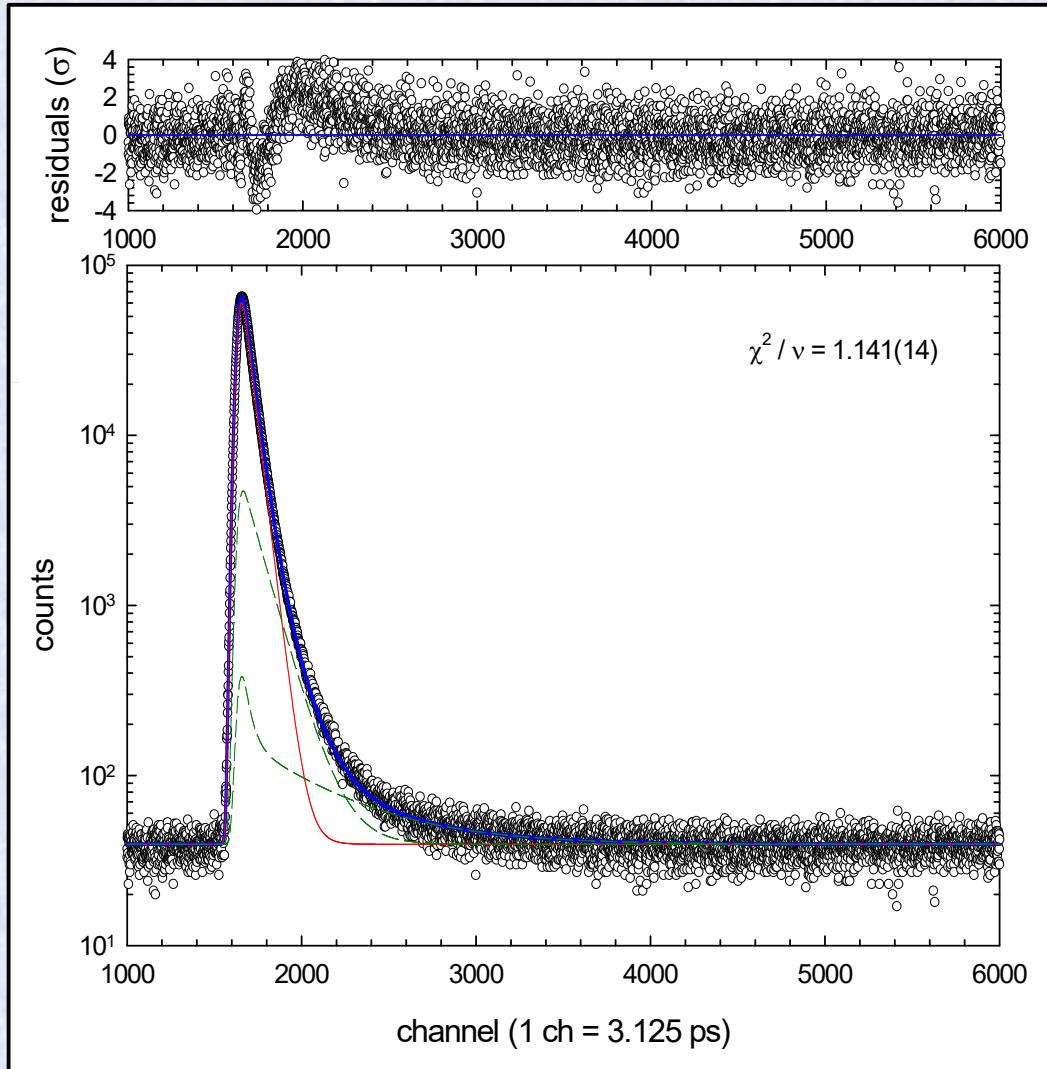
## Fitting of LT spectrum

- 100Cr6 roll bearing steel



- single component fit

$$\tau_1 = 155.7(1) \text{ ps}$$



## Fitting of LT spectrum

- 100Cr6 roll bearing steel

- $\chi^2$  test

$$\chi^2 = \frac{\sum_{i=1}^m (y_i - h(x_i|\theta))^2}{h(x_i|\theta)}$$

- $\chi^2$  per degree of freedom:  $\chi^2 / \nu$

- expectation value: 1

- variance:  $\sigma^2 = 2 / \nu$

- number of degrees of freedom

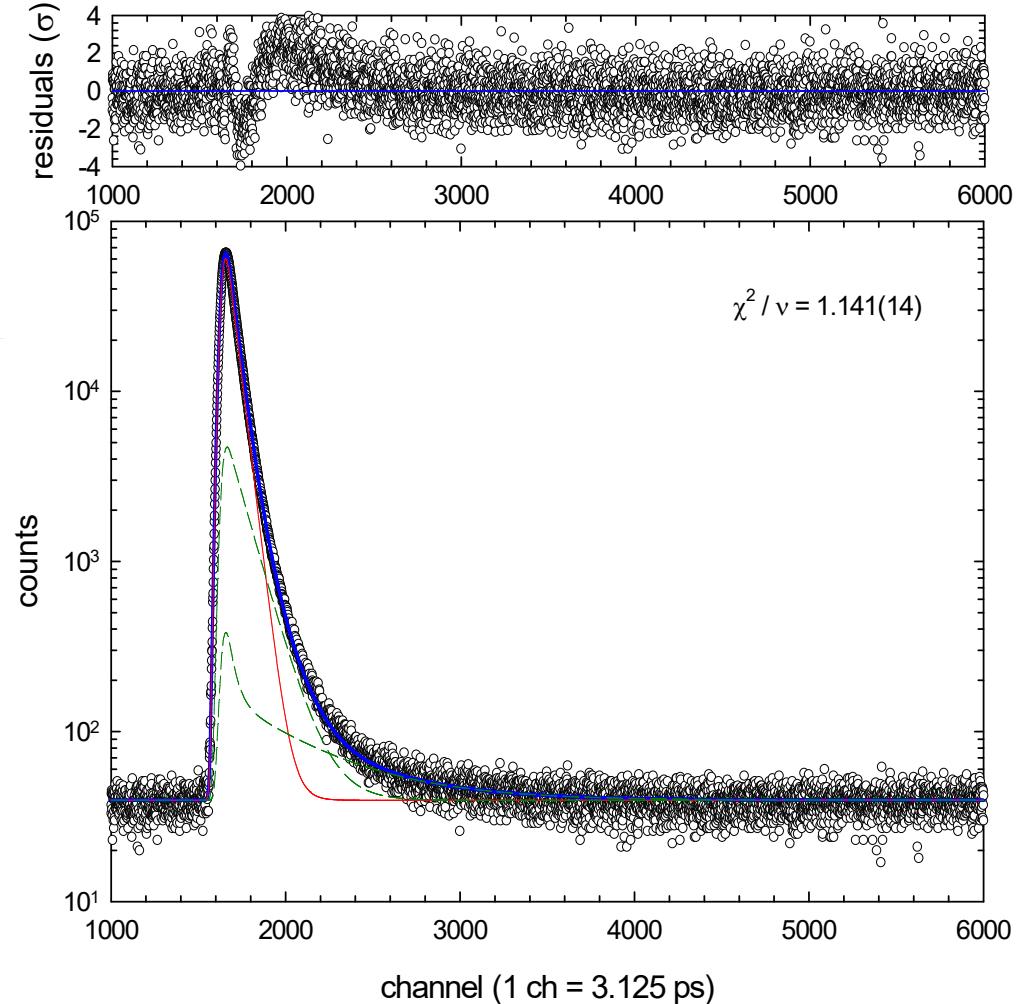
$$\nu = m - p$$

number of channels

number of fitting parameters

- single component fit

$$\tau_1 = 155.7(1) \text{ ps}$$



## Fitting of LT spectrum

- 100Cr6 roll bearing steel

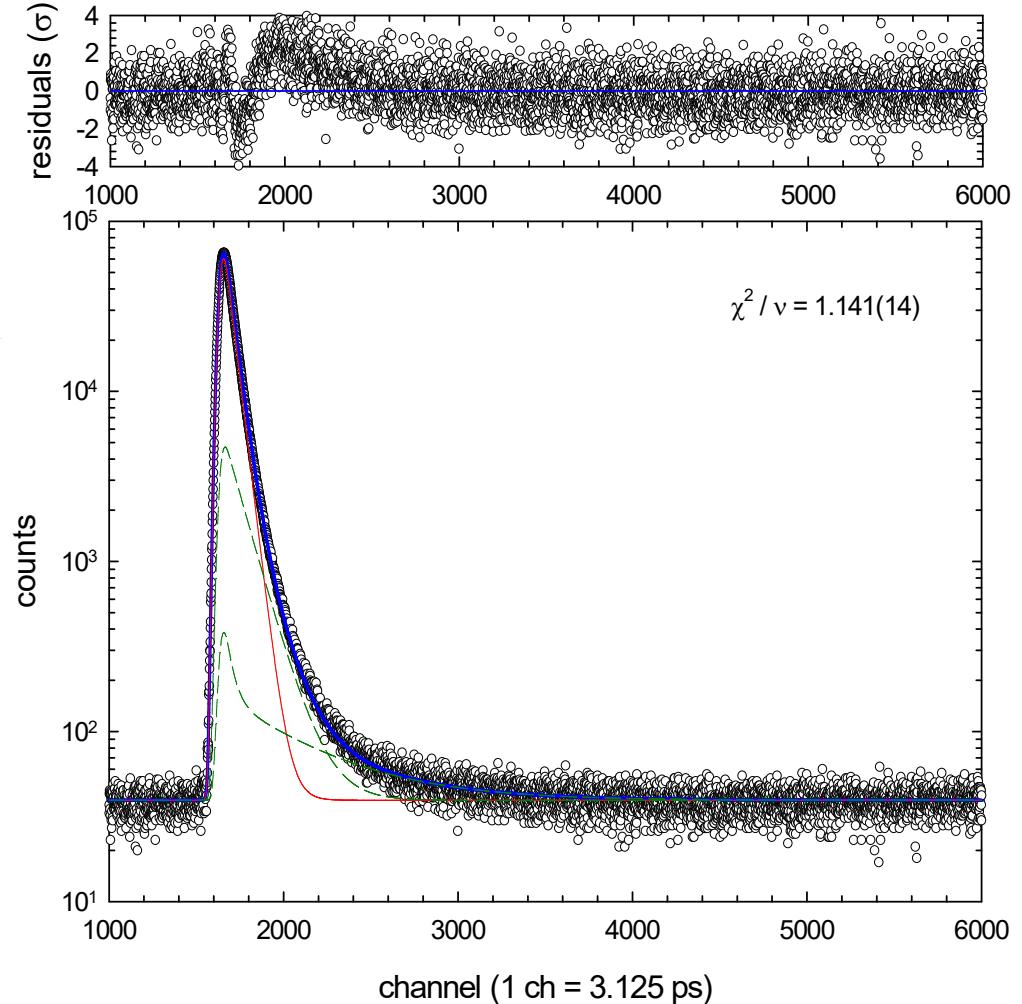
- residuals

$$r = \frac{\sum_{i=1}^m (y_i - h(x_i | \theta))}{\sqrt{h(x_i | \theta)}}$$

- $r$  has normal distribution
- expectation value: 0
- variance:  $\sigma^2 = 1$

- single component fit

$$\tau_1 = 155.7(1) \text{ ps}$$



## Fitting of LT spectrum

- 100Cr6 roll bearing steel

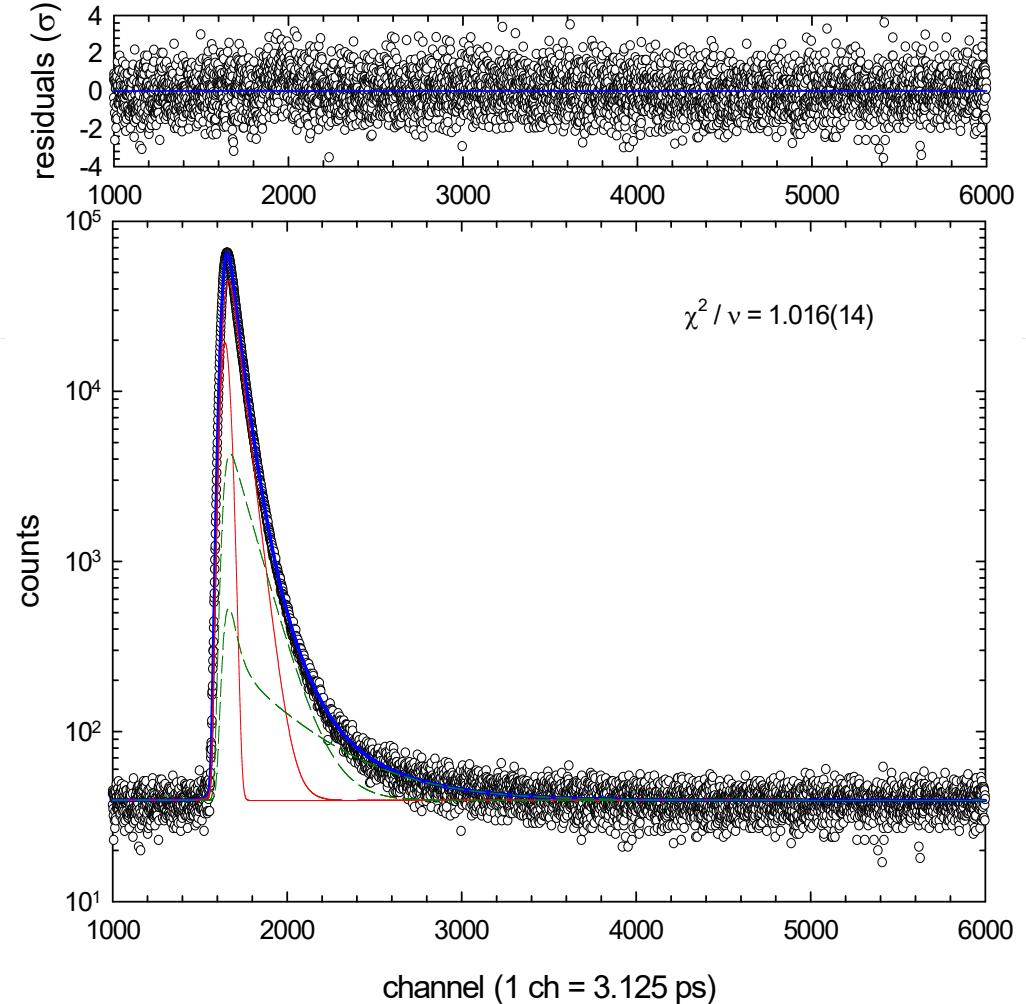
- two-component fit

$$\begin{aligned}\tau_1 &= 20(5) \text{ ps}, I_1 = 19(6)\%, \\ \tau_2 &= 156(3) \text{ ps}, I_2 = 81(5)\%\end{aligned}$$

- residuals

$$r = \frac{\sum_{i=1}^m (y_i - h(x_i | \theta))}{\sqrt{h(x_i | \theta)}}$$

- $r$  has normal distribution
- expectation value: 0
- variance:  $\sigma^2 = 1$



## LT spectrum

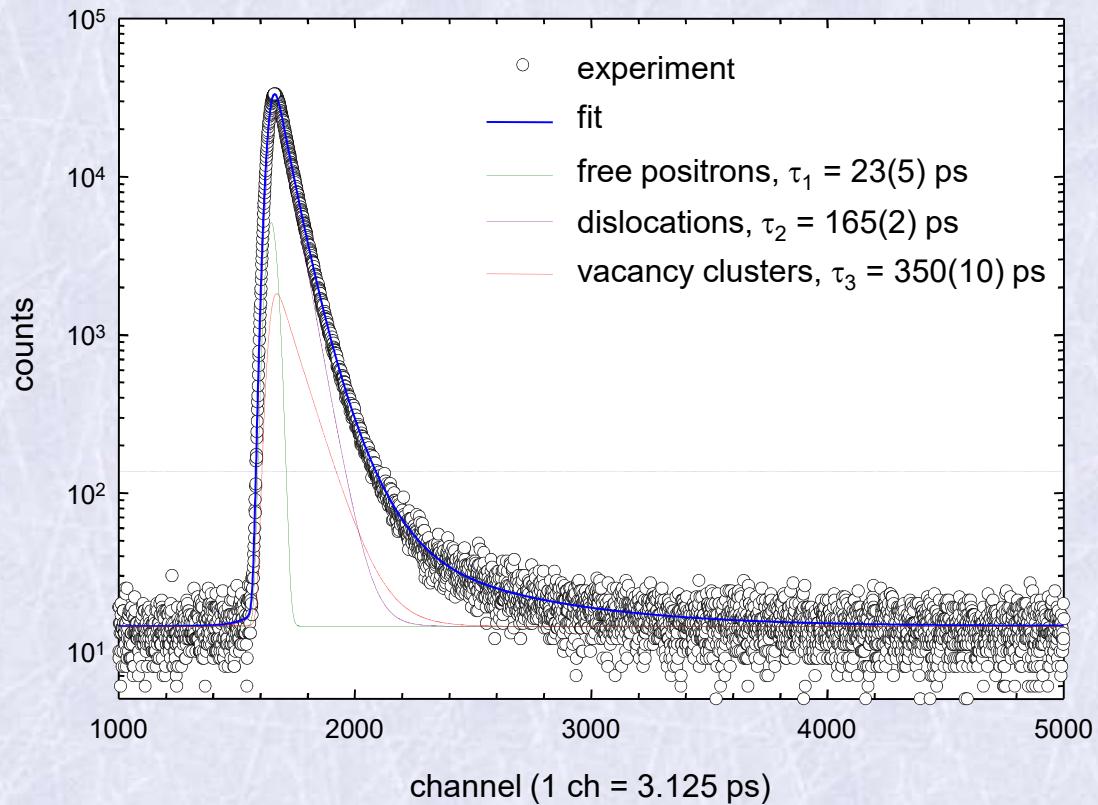
$N$  type of defects



$N+1$  components

$$S_{\text{id}} = \sum_{i=1}^{N+1} \frac{1}{\tau_i} I_i e^{-\frac{t}{\tau_i}}$$

LT spectrum of heavily deformed Nb



decomposition of LT spectrum

lifetimes  $\tau_i \rightarrow$  type of defects

intensities  $I_i \rightarrow$  defect concentrations

## LT spectroscopy

- fitting of LT spectrum



- lifetimes  $\tau_i$  and intensities  $I_i$  of exponential components



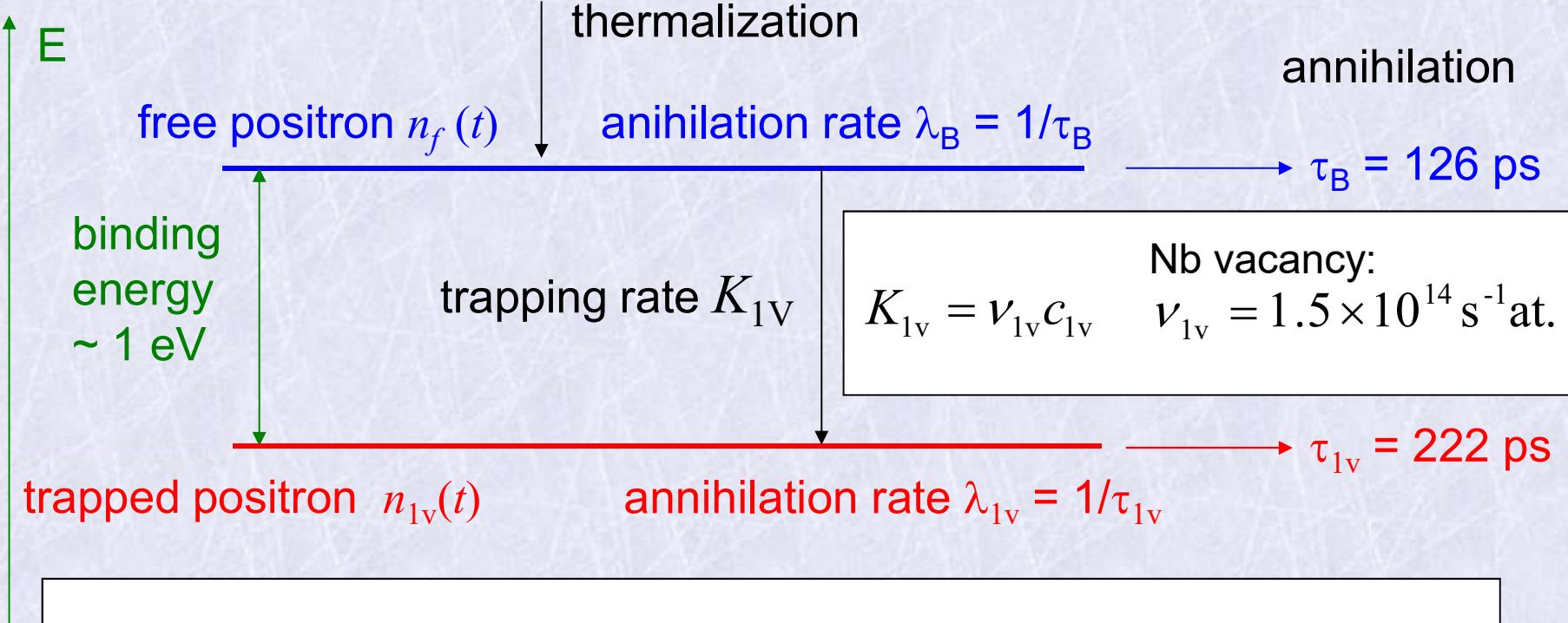
- (comparison with *ab-initio* theoretical calculations) —→ identification of defects



- application of positron trapping model —→ determination of defect concentrations

## Simple trapping model (STM)

Nb with vacancies

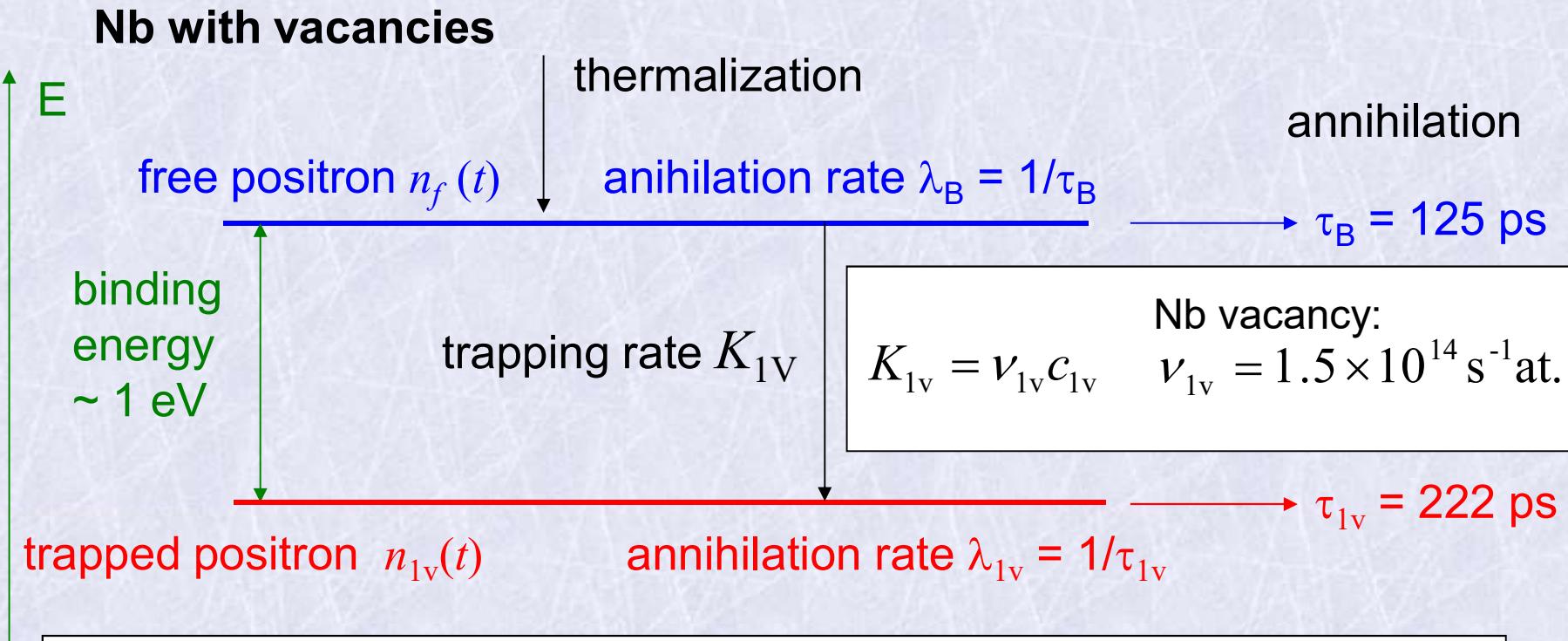


assumptions:

1. single type of defects
2. uniform distribution of defects
3. only thermalized  $e^+$  are trapped
4. no detrapping

R.N. West Adv. Phys. 22, 263 (1973)

## Simple trapping model (STM)



$$\frac{dn_f}{dt} = -\lambda_B n_f - K_{1v} n_f$$

$n_f(t)$  ..... probability that  $e^+$  is in the free state at time  $t$

$$\frac{dn_{1v}}{dt} = -\lambda_{1v} n_{1v} + K_{1v} n_f$$

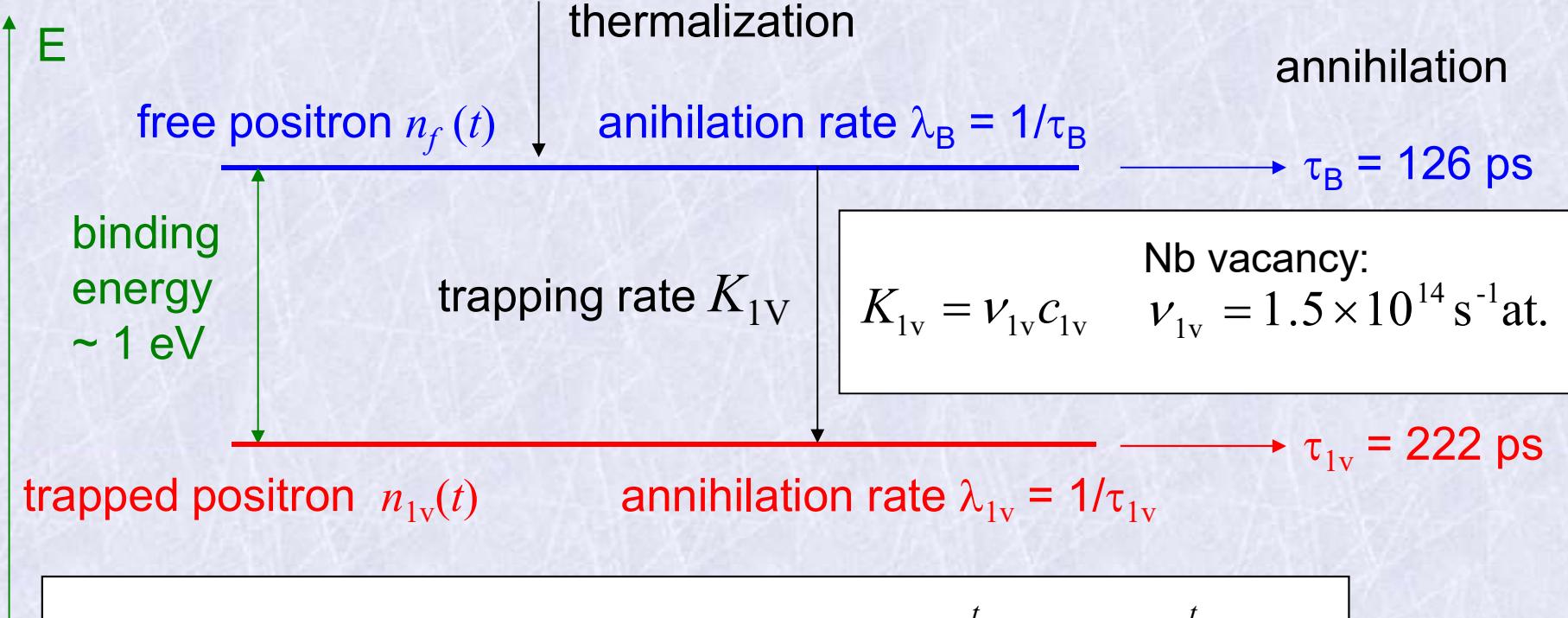
$n_{1v}(t)$  ..... probability that  $e^+$  is in trapped state at time  $t$

$$n_{1v}(t=0)=0 \quad n_f(t=0)=1$$

R.N. West Adv. Phys. 22, 263 (1973)

## Simple trapping model (STM)

Nb with vacancies



two-component spectrum:

$$S_{\text{id}} = \frac{1}{\tau_1} I_1 e^{-\frac{t}{\tau_1}} + \frac{1}{\tau_2} I_2 e^{-\frac{t}{\tau_2}}$$

$$\tau_1 = \frac{1}{\lambda_B + K_{1v}}$$

$$I_1 = 1 - I_2$$

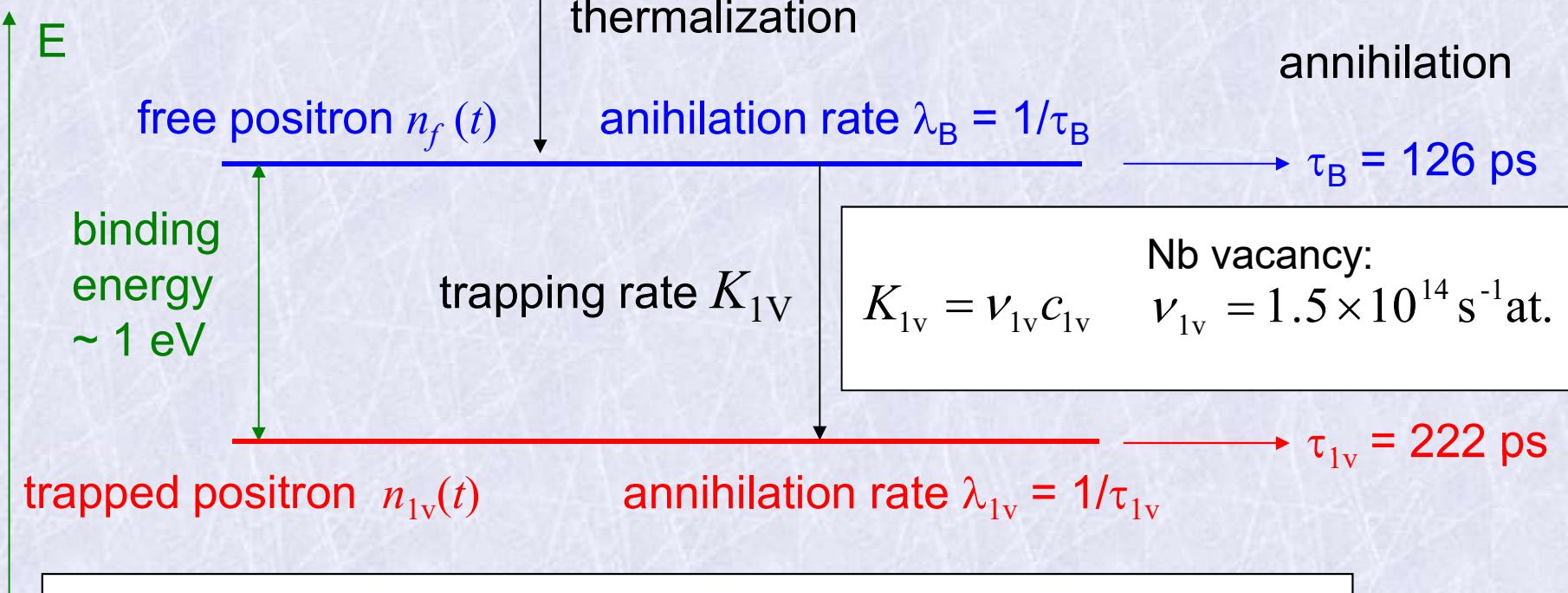
free positrons

$$\tau_2 = \frac{1}{\lambda_{1v}} \quad I_2 = \frac{K_{1v}}{\lambda_B + K_{1v} - \lambda_{1v}}$$

positrons trapped  
in vacancies

## Simple trapping model (STM)

Nb with vacancies



$$\text{trapping rate: } K_{1V} = \frac{I_2}{I_1} (\lambda_B - \lambda_{1V}) = I_2 \left( \frac{1}{\tau_1} - \frac{1}{\tau_2} \right)$$

$$\text{concentration of vacancies: } c_{1V} = \frac{K_{1V}}{\nu_{1V}}$$

## Simple trapping model (STM)

### Nb with vacancies

- check whether STM assumptions are fulfilled

$$\tau_1 = \frac{1}{\lambda_B + K_{1v}} \quad I_1 = 1 - I_2 \quad \text{free positrons}$$

$$\tau_2 = \frac{1}{\lambda_{1v}} \quad I_2 = \frac{K_{1v}}{\lambda_B + K_{1v} - \lambda_{1v}} \quad \text{positrons trapped in vacancies}$$

$$\tau_B = \left( \frac{I_1}{\tau_1} + \frac{I_2}{\tau_2} \right)^{-1}$$

- for example: electron irradiated Nb

$$\tau_1 = 78(3) \text{ ps}, I_1 = 46(2) \%$$

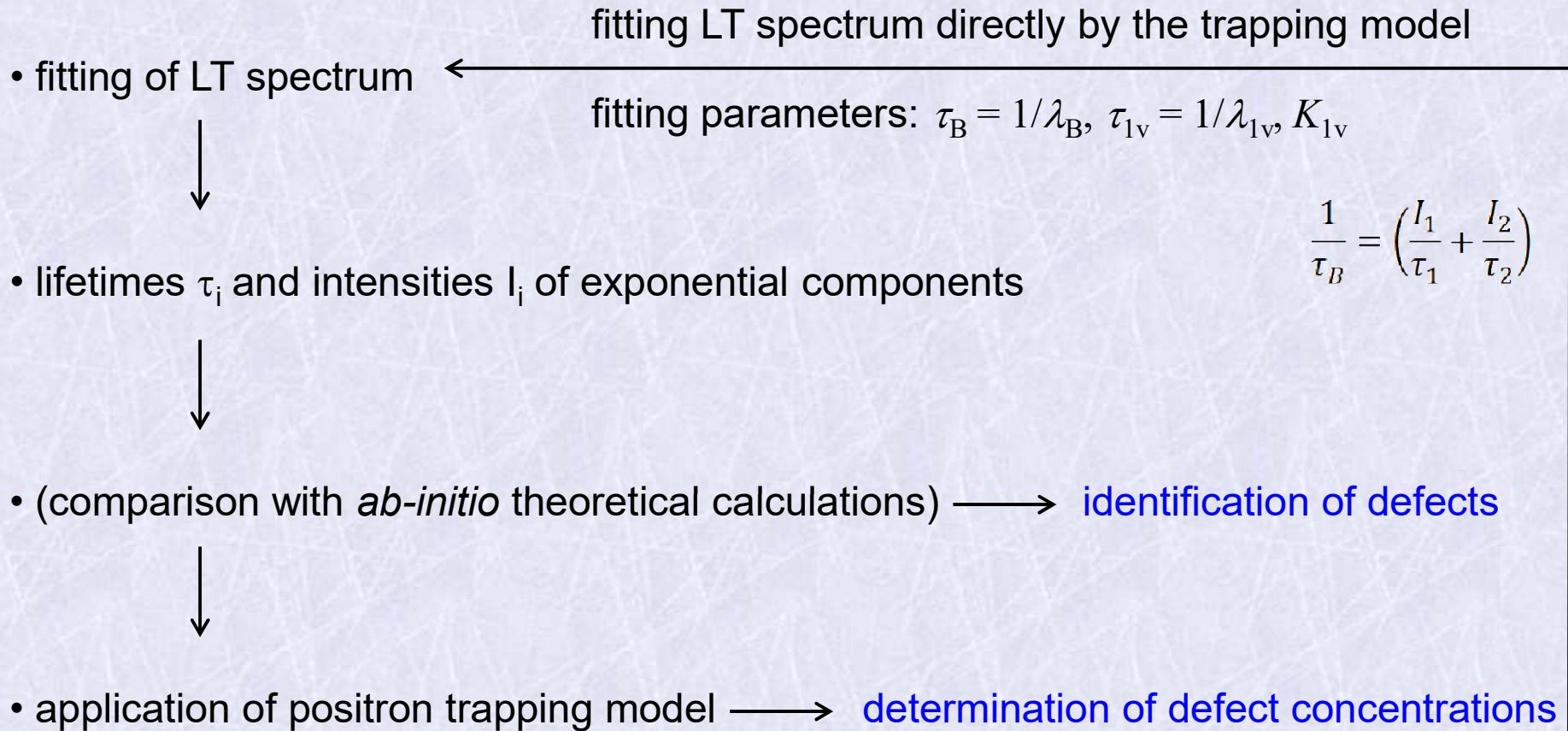
$$\tau_f = (I_1/\tau_1 + I_2/\tau_2)^{-1} = 124(4) \text{ ps}$$

$$\tau_2 = 217(5) \text{ ps}, I_2 = 64(2) \%$$

vacancy concentration:  $c_{1V} = 32(5) \text{ ppm}$

- defect-free Nb reference:  $\tau_B = 125(1) \text{ ps}$

## LT spectroscopy



$$\tau_1 = \frac{1}{\lambda_B + K_{1v}} \quad I_1 = 1 - I_2$$

free positrons

$$\tau_2 = \frac{1}{\lambda_{1v}} \quad I_2 = \frac{K_{1v}}{\lambda_B + K_{1v} - \lambda_{1v}}$$

positrons trapped  
in vacancies

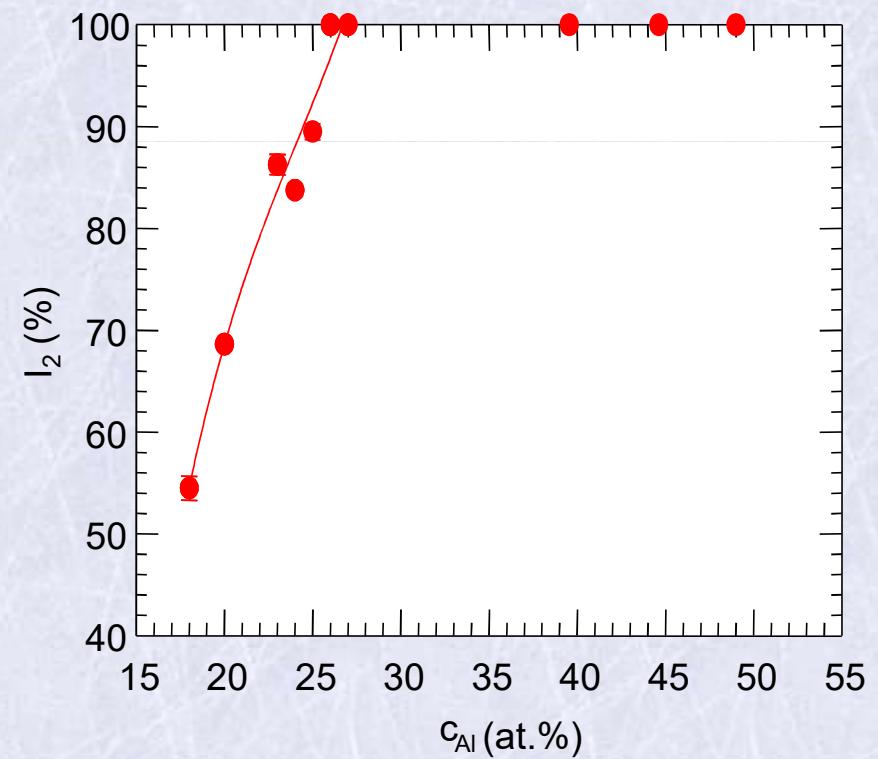
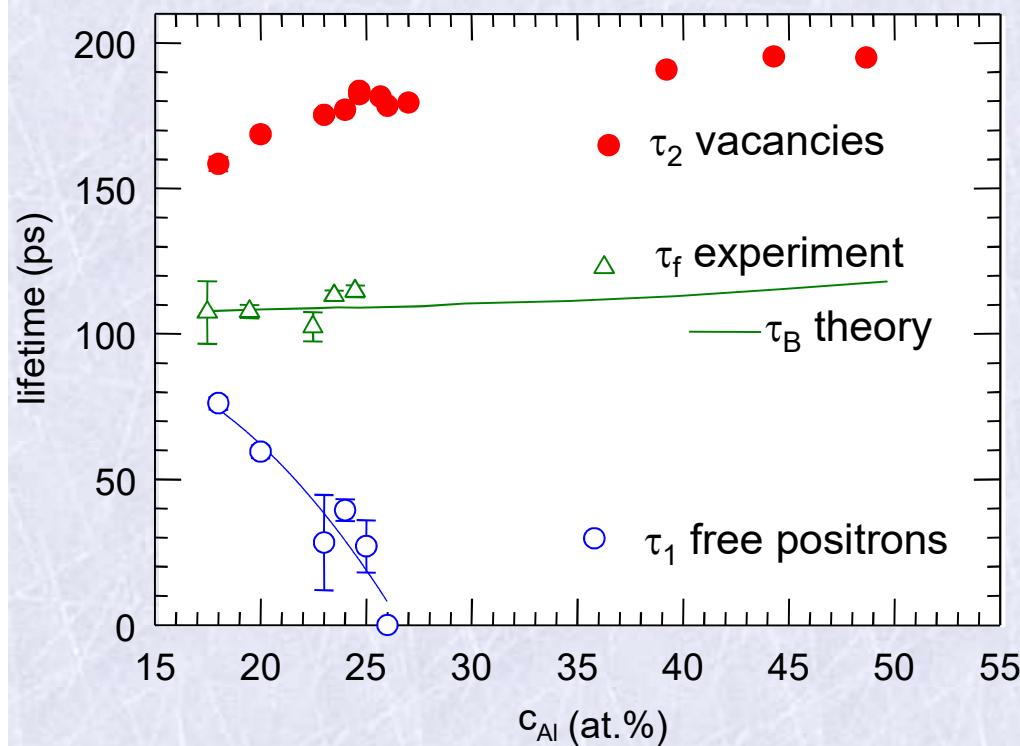
$$S_{id} = \frac{1}{\tau_1} I_1 e^{-\frac{t}{\tau_1}} + \frac{1}{\tau_2} I_2 e^{-\frac{t}{\tau_2}}$$

model LT spectrum

## Simple trapping model (STM)

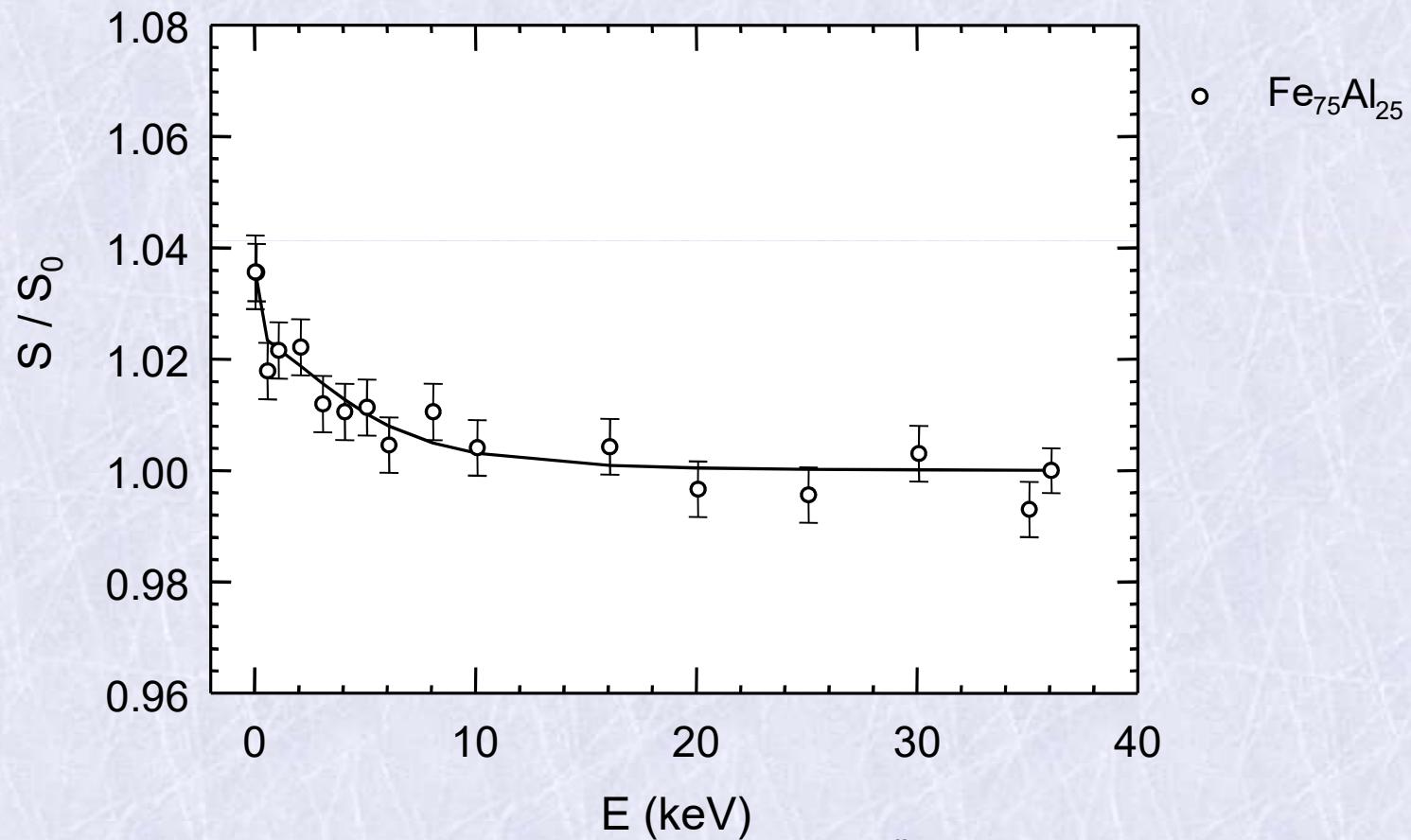
### Fe-Al alloys

- quenched from 1000°C
  - two component LT spectrum:  
 $\tau_1$  – free positrons  
 $\tau_2$  – positrons trapped at quenched-in vacancies
- $c_{Al} \geq 26$  at.% → saturated trapping



## Positron back-diffusion measurement

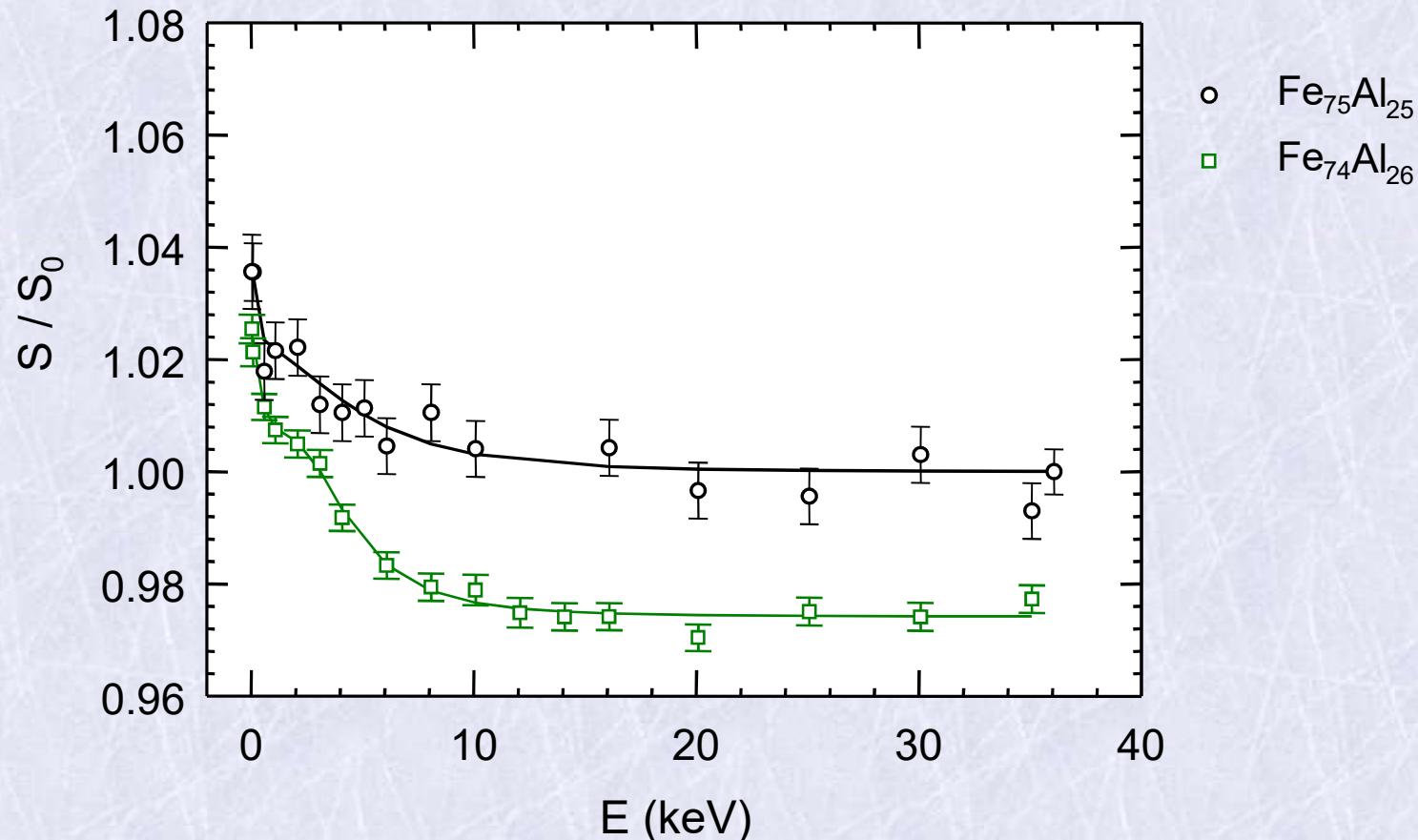
Fe-Al alloys quenched from 1000°C – dependence of S parameter on  $e^+$  energy



J. Čížek et al., Phys. B 407, 2659 (2012)

## Positron back-diffusion measurement

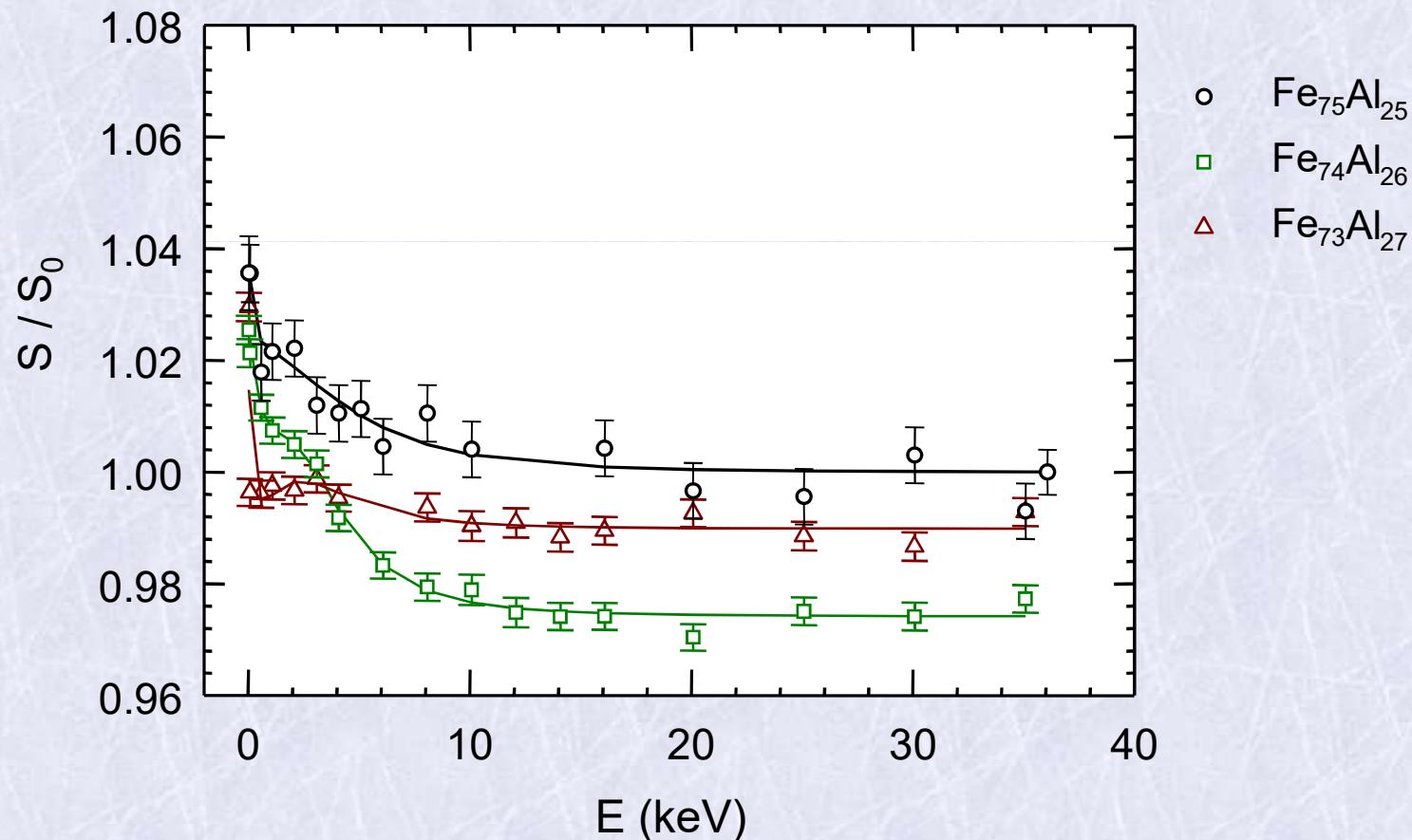
Fe-Al alloys quenched from 1000°C – dependence of S parameter on  $e^+$  energy



J. Čížek et al., Phys. B 407, 2659 (2012)

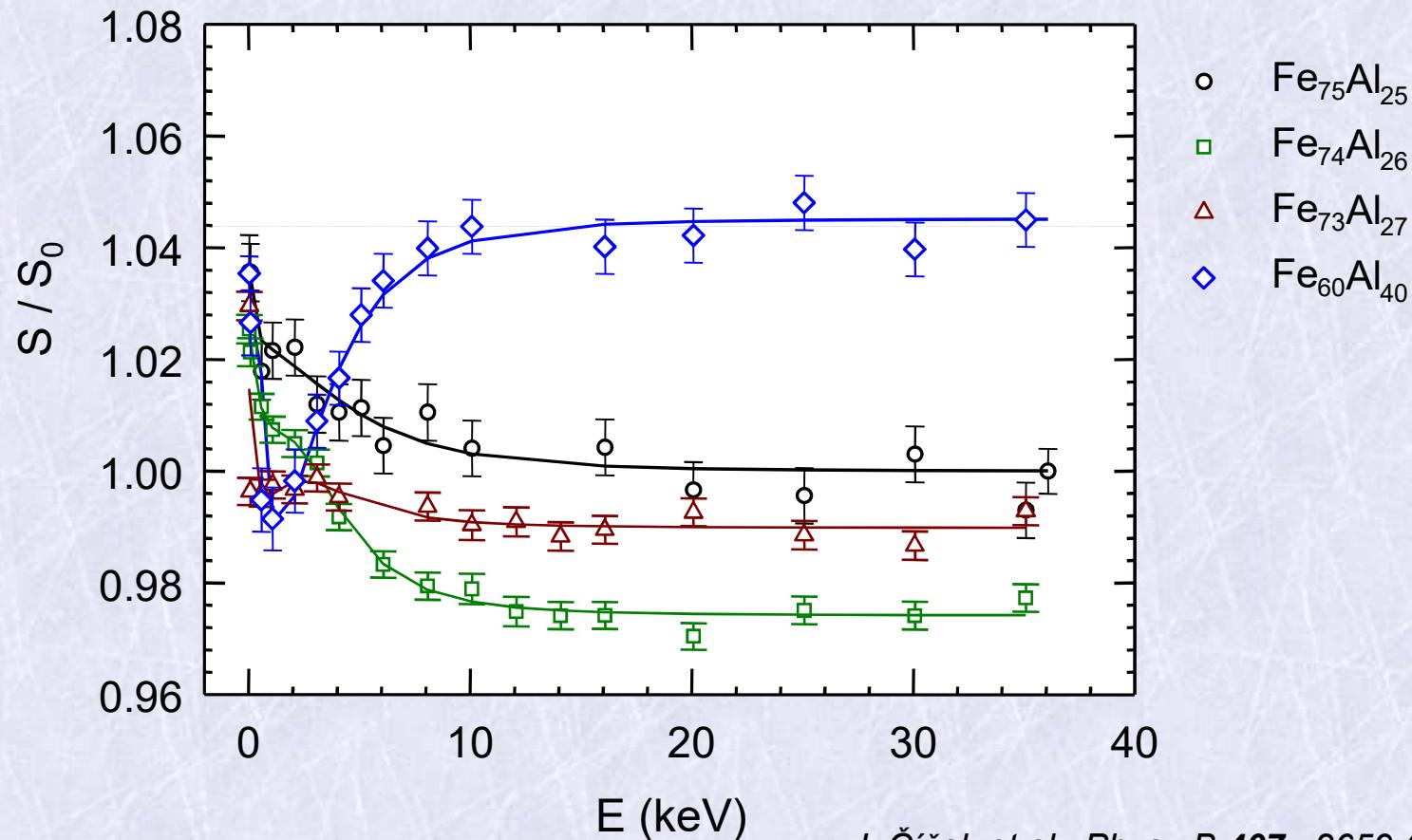
## Positron back-diffusion measurement

Fe-Al alloys quenched from 1000°C – dependence of S parameter on e<sup>+</sup> energy



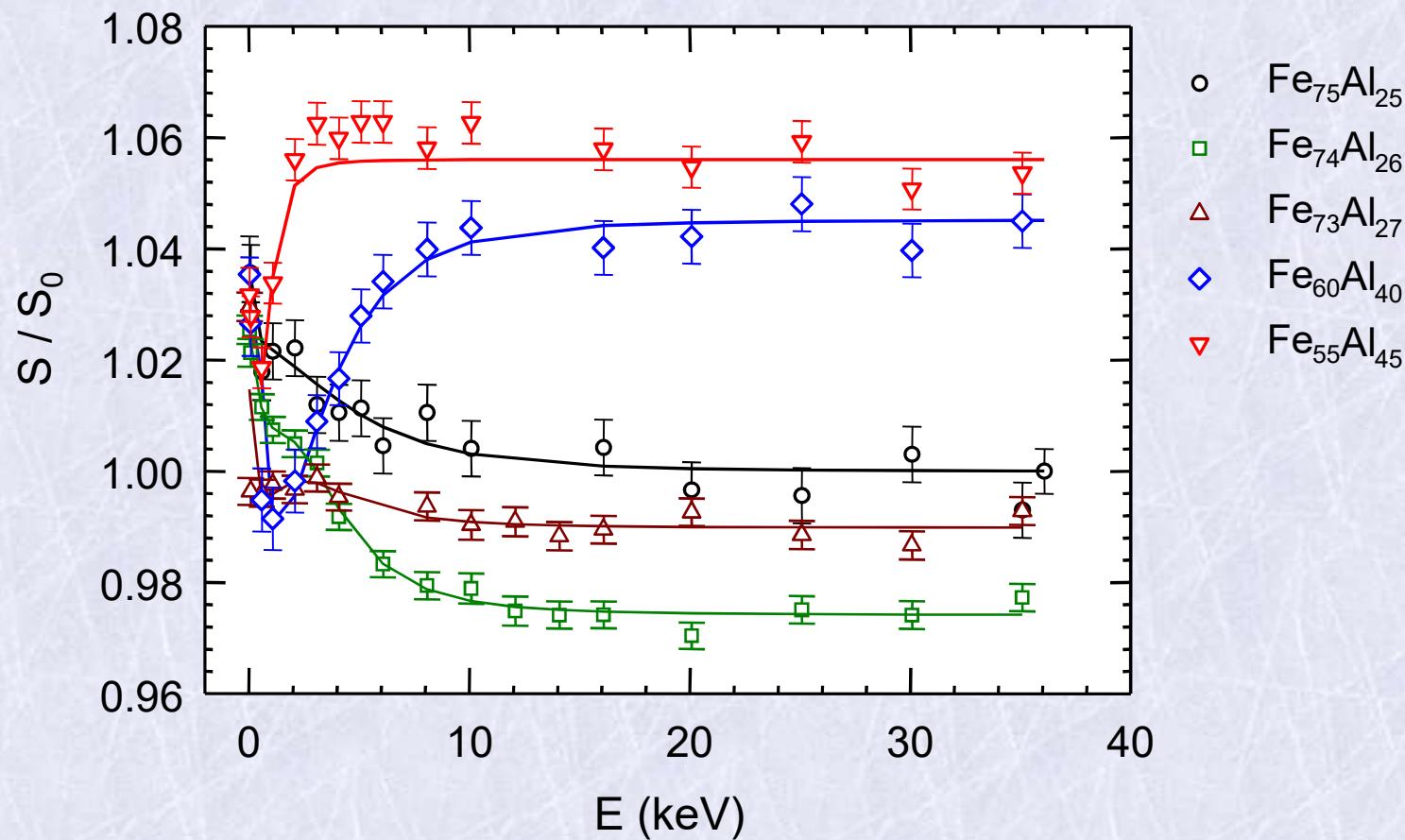
## Positron back-diffusion measurement

Fe-Al alloys quenched from 1000°C – dependence of S parameter on e<sup>+</sup> energy



## Positron back-diffusion measurement

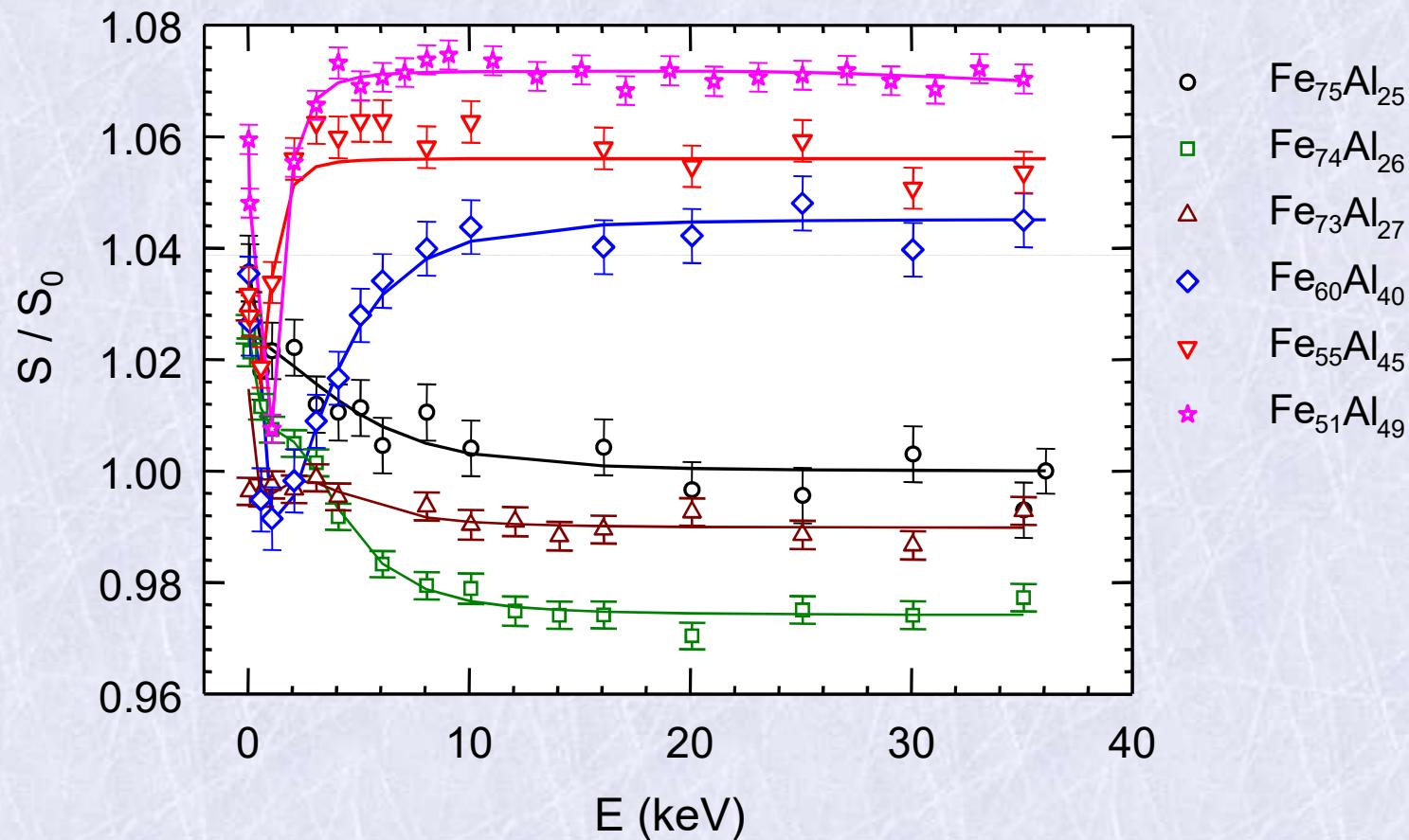
Fe-Al alloys quenched from 1000°C – dependence of S parameter on  $e^+$  energy



## Positron back-diffusion measurement

### Fe-Al alloys quenched from 1000°C – dependence of S parameter on $e^+$ energy

- solid lines – model curves calculated by VEPFIT
- two layered model: (i) surface oxide layer 15-20 nm (ii) bulk Fe-Al alloy



## Positron back-diffusion measurement

- positron diffusion length  $L_+$

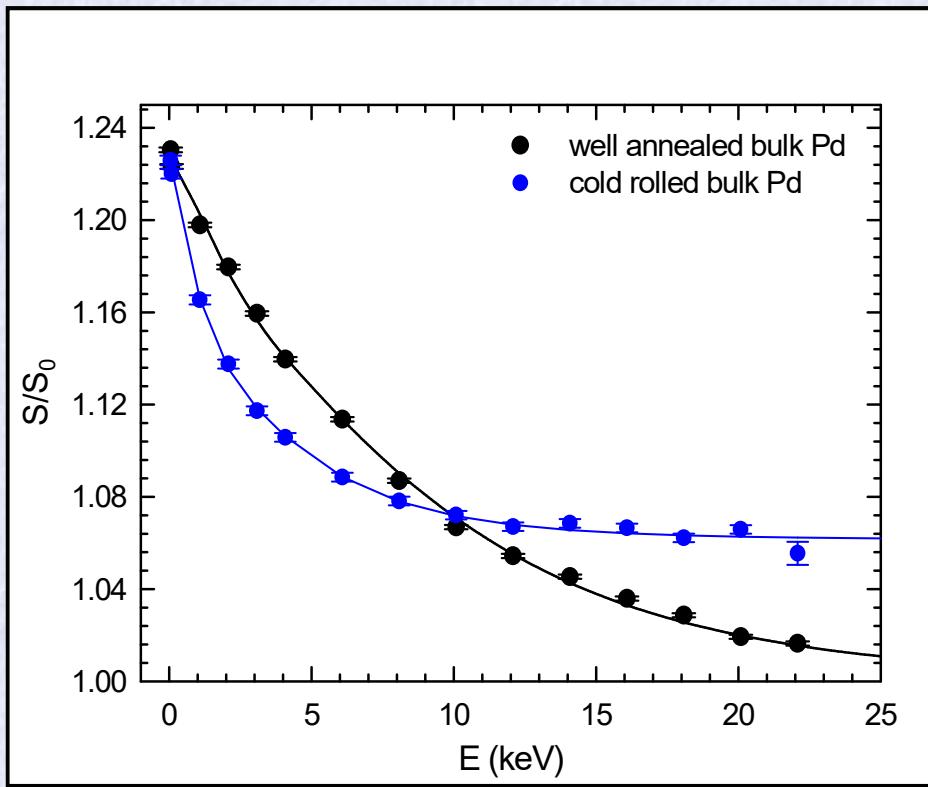
- perfect lattice:  $L_{+,B} = \sqrt{D_+ \tau_B}$

$D_+$  - positron diffusion coefficient

$\tau_B$  – bulk positron lifetime

- presence of defects  $\rightarrow$  shortening of  $L_+$

$$L_+ = \sqrt{D_+ \tau_I} \quad \tau_I \text{ – lifetime of the free positron component } (\tau_I < \tau_B)$$



## Positron back-diffusion measurement

- positron diffusion length  $L_+$
- perfect lattice:  $L_{+,B} = \sqrt{D_+ \tau_B}$   
 $D_+$  - positron diffusion coefficient  
 $\tau_B$  – bulk positron lifetime
- presence of defects  $\rightarrow$  shortening of  $L_+$      $L_+ = \sqrt{D_+ \tau_1}$      $\tau_1$  – lifetime of the free positron component
- simple trapping model:  $\tau_1 = \frac{1}{\frac{1}{\tau_B} + K}$
- positron trapping rate to defects:  $K = \frac{1}{\tau_B} \left( \frac{L_{+,B}^2}{L_+^2} - 1 \right)$
- net concentration of defects:  
$$c = \frac{K}{v} = \frac{1}{v \tau_B} \left( \frac{L_{+,B}^2}{L_+^2} - 1 \right)$$

## Positron back-diffusion measurement

- positron lifetime measurement

$$c = \frac{1}{\nu} \frac{I_2}{I_1} \left( \frac{1}{\tau_B} - \frac{1}{\tau_2} \right) = \frac{1}{\nu} I_2 \left( \frac{1}{\tau_1} - \frac{1}{\tau_2} \right)$$

- It is hard to resolve free positron component when  $I_f < 5\%$  (saturated trapping)
- in FeAl alloys it corresponds  $c > 2 \times 10^{-4} = 200 \text{ ppm}$

- positron back-diffusion measurement

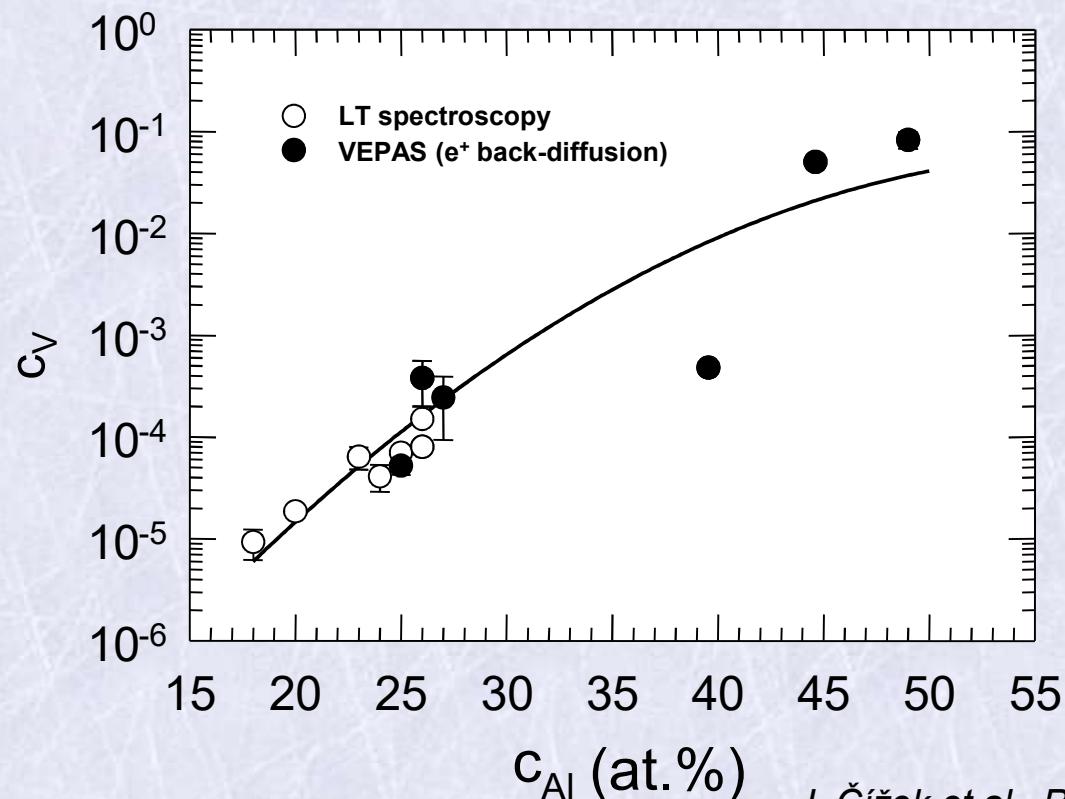
$$c = \frac{K}{\nu} = \frac{1}{\nu \tau_B} \left( \frac{L_{+,B}^2}{L_+^2} - 1 \right)$$

- It is hard to determine positron diffusion length when  $L_+ < 1 \text{ nm}$
- in FeAl alloys it corresponds  $c > 1 \times 10^{-3} = 10 \text{ at.\%} = 10^5 \text{ ppm}$
- positron back-diffusion measurement can be used for determination of defect concentration when LT spectroscopy cannot be used because of saturated trapping

## Concentration of quenched-in vacancies

### Fe-Al alloys quenched from 1000°C

- LT spectroscopy and VEPAS gave mutually consistent results
- Fe<sub>75</sub>Al<sub>25</sub> alloy: LT spectroscopy:  $c_V = (7.0 \pm 0.5) \times 10^{-5}$   
VEPAS (e<sup>+</sup> back-diffusion):  $c_V = (5 \pm 1) \times 10^{-5}$

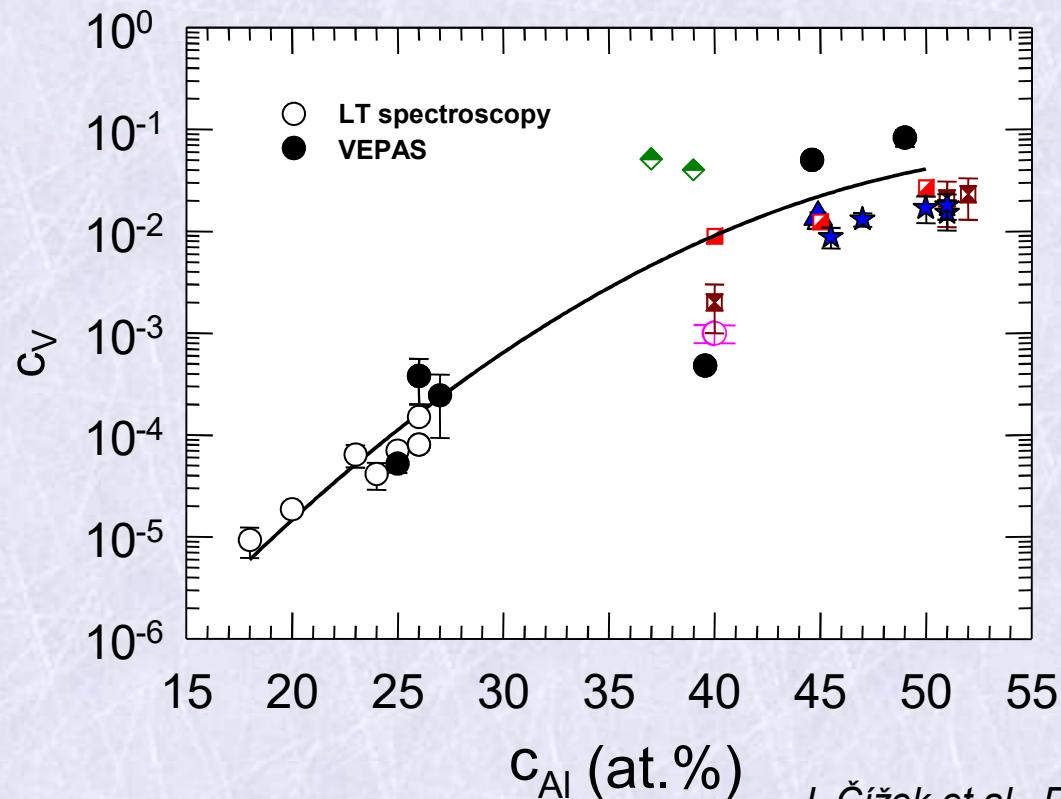


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## Concentration of quenched-in vacancies

Fe-Al alloys quenched from 1000°C

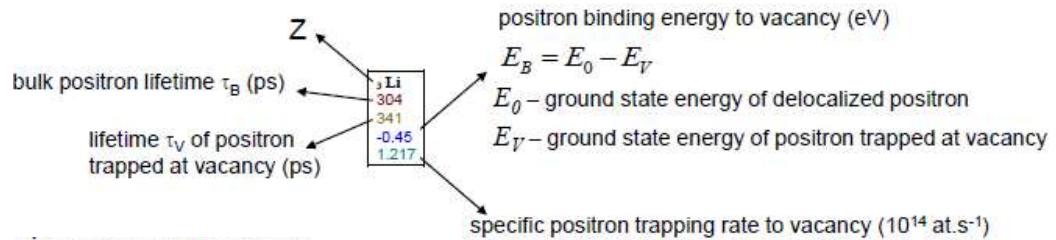
- ▲ T. Haraguchi 2001, LT spectroscopy
- ◆ R. Würschum 1995, in-situ LT spectroscopy
- Y.A. Chang 1993, microhardness + theoretical modeling
- J. Joardar 2005, dilatometry + XRD
- D. Paris 1977, dilatometry + XRD
- ★ K. Ho 1978, dilatometry + XRD



# Vacancies

$$c_{1V} = \frac{K_{1V}}{\nu_{1V}}$$

- calculated specific  $e^+$  trapping rates for vacancies



	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
1	${}^1\text{H}$																${}^2\text{He}$	
2	${}^3\text{Li}$ 304 341 -0.45 1.217	${}^4\text{Be}$															${}^{10}\text{Ne}$	
3	${}^{11}\text{Na}$ 328 365 -0.20 0.362	${}^{12}\text{Mg}$															${}^{18}\text{Ar}$	
4	${}^{19}\text{K}$ 374 414 -0.31 0.177	${}^{20}\text{Ca}$	${}^{21}\text{Sc}$	${}^{22}\text{Ti}$	${}^{23}\text{V}$ 117 200 -4.01 6.077	${}^{24}\text{Cr}$ 107 184 -3.11 6.247	${}^{25}\text{Mn}$	${}^{26}\text{Fe}$ 102 177 -3.29 6.779	${}^{27}\text{Co}$	${}^{28}\text{Ni}$ 97 166 -2.74 6.156	${}^{29}\text{Cu}$ 109 170 -1.24 3.817	${}^{30}\text{Zn}$	${}^{31}\text{Ga}$	${}^{32}\text{Ge}$	${}^{33}\text{As}$	${}^{34}\text{Se}$	${}^{35}\text{Br}$	${}^{36}\text{Kr}$
5	${}^{37}\text{Rb}$ 376 419 -0.35 0.155	${}^{38}\text{Sr}$ 310 387 -0.97 0.407	${}^{39}\text{Y}$	${}^{40}\text{Zr}$	${}^{41}\text{Nb}$ 126 222 -3.65 4.103	${}^{42}\text{Mo}$ 108 199 -3.94 5.150	${}^{43}\text{Tc}$	${}^{44}\text{Ru}$	${}^{45}\text{Rh}$ 97 179 -2.95 4.677	${}^{46}\text{Pd}$ 107 173 -1.11 2.634	${}^{47}\text{Ag}$ 125 200 -1.16 2.215	${}^{48}\text{Cd}$	${}^{49}\text{In}$	${}^{50}\text{Sn}$	${}^{51}\text{Sb}$	${}^{52}\text{Te}$	${}^{53}\text{I}$	${}^{54}\text{Xe}$
6	${}^{85}\text{Cs}$ 392 431 -0.42 0.113	${}^{86}\text{Ba}$ 305 393 -1.39 0.461	${}^{71}\text{Lu}$	${}^{72}\text{Hf}$	${}^{73}\text{Ta}$ 118 217 -4.19 4.392	${}^{74}\text{W}$	${}^{75}\text{Re}$	${}^{76}\text{Os}$	${}^{77}\text{Ir}$ 90 175 -4.03 5.301	${}^{78}\text{Pt}$ 98 181 -2.48 3.738	${}^{79}\text{Au}$ 112 191 -1.51 2.496	${}^{80}\text{Hg}$	${}^{81}\text{Tl}$	${}^{82}\text{Pb}$ 191 277 -0.79 0.841	${}^{83}\text{Bi}$	${}^{84}\text{Po}$	${}^{85}\text{At}$	${}^{86}\text{Rn}$
7	${}^{87}\text{Fr}$	${}^{88}\text{Ra}$	${}^{103}\text{Lr}$	${}^{104}\text{Rf}$	${}^{105}\text{Db}$	${}^{107}\text{Sg}$	${}^{107}\text{Bh}$											
			${}^{57}\text{La}$	${}^{58}\text{Ce}$	${}^{59}\text{Pr}$	${}^{60}\text{Nd}$	${}^{61}\text{Pm}$	${}^{62}\text{Sm}$	${}^{63}\text{Eu}$ 270 364 -1.28 0.638	${}^{64}\text{Gd}$	${}^{65}\text{Tb}$	${}^{66}\text{Dy}$	${}^{67}\text{Ho}$	${}^{68}\text{Er}$	${}^{69}\text{Tm}$	${}^{70}\text{Yb}$		
			${}^{89}\text{Ac}$	${}^{90}\text{Th}$	${}^{91}\text{Pa}$	${}^{92}\text{U}$	${}^{93}\text{Np}$	${}^{94}\text{Pu}$	${}^{95}\text{Am}$	${}^{96}\text{Cm}$	${}^{97}\text{Bk}$	${}^{98}\text{Cf}$	${}^{99}\text{Es}$	${}^{100}\text{Fm}$	${}^{101}\text{Md}$	${}^{102}\text{No}$		

## Vacancies

- calculated specific positron trapping rates: comparison with experiment

element	calculated (LDA) $\nu (10^{14}) \text{ at.s}^{-1}$	experimental $\nu (10^{14}) \text{ at.s}^{-1}$	method	Reference
Al	3.139	$2.5 \pm 1.5$ $2.5 \pm 1.0$ $3 \pm 2$	thermal vac. thermal vac. thermal vac.	E. Gramsch, K.G. Lynn, <i>Phys. Rev. B</i> <b>40</b> (1989) 2537 J. A. Jackman, G. M. Hood and R. J. Schultz, <i>J. Phys. F</i> <b>17</b> (1987) 1817 T.M. Hall, A.N. Goland, C.N. Snead Jr., <i>Phys. Rev. B</i> <b>10</b> (1974) 3062.
Fe	6.779	$11 \pm 2$	$e^-$ irrad.	A. Vehanen, P. Hautojärvi, J. Johansson, J. Yli-Kauppila, P. Moser, <i>Phys. Rev. B</i> <b>25</b> (1982) 762
Cu	3.817	$1.4 \pm 0.2$	$\Delta l/l - \Delta a/a$	J.-E. Kluin, Th. Hehenkamp, <i>Phys. Rev. B</i> <b>44</b> (1991) 11597
Ag	2.215	$2.3 \pm 0.2$	$\Delta l/l - \Delta a/a$	J. Wolff, J.-E. Kluin, Th. Hehenkamp, <i>Mater. Sci. Forum</i> <b>105-110</b> (1992) 1329
Au	2.496	$3.5 \pm 1.0$ $2.9 \pm 0.8$	thermal vac. thermal vac.	T.M. Hall, A.N. Goland, C.N. Snead Jr., <i>Phys. Rev. B</i> <b>10</b> (1974) 3062 T.M. Hall, A.N. Goland, K.C. Jain, R.W. Siegel, <i>Phys. Rev. B</i> <b>12</b> (1975) 1613

- Thermal vacancies

$$c_V = \exp\left(\frac{S_f}{k}\right) \exp\left(-\frac{H_f}{kT}\right)$$

$H_f$  - vacancy formation enthalpy

$S_f$  - vacancy formation entropy  $S_f = (2-3) k$

$k$  - Boltzmann constant

## Vacancies

- calculated specific positron trapping rates: comparison with experiment

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- simultaneous measurement of length change  $\Delta l / l$  (differential dilatometry) and change of the lattice parameter  $\Delta a / a$  (X-ray diffraction)

$$c_v = 3 \left( \frac{\Delta l}{l} - \frac{\Delta a}{a} \right)$$

## Vacancies

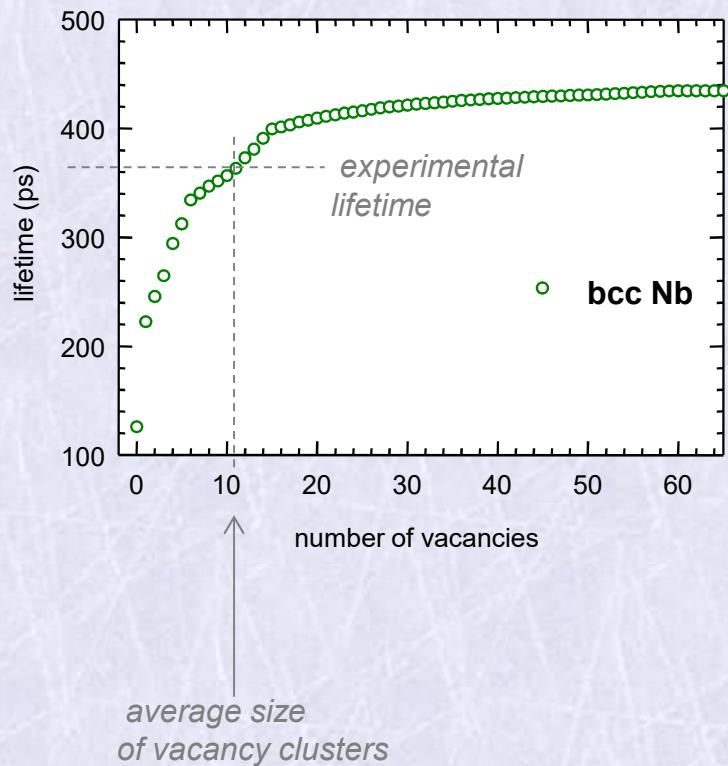
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Fe	6.779	$11 \pm 2$	e <sup>-</sup> irrad.	A. Vehanen, P. Hautojärvi, J. Johansson, J. Yli-Kauppila, P. Moser, <i>Phys. Rev. B</i> <b>25</b> (1982) 762
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- specific trapping rate for vacancies in metals:  $\nu_V = 10^{14}\text{-}10^{15} \text{ at.s}^{-1}$

## vacancy clusters

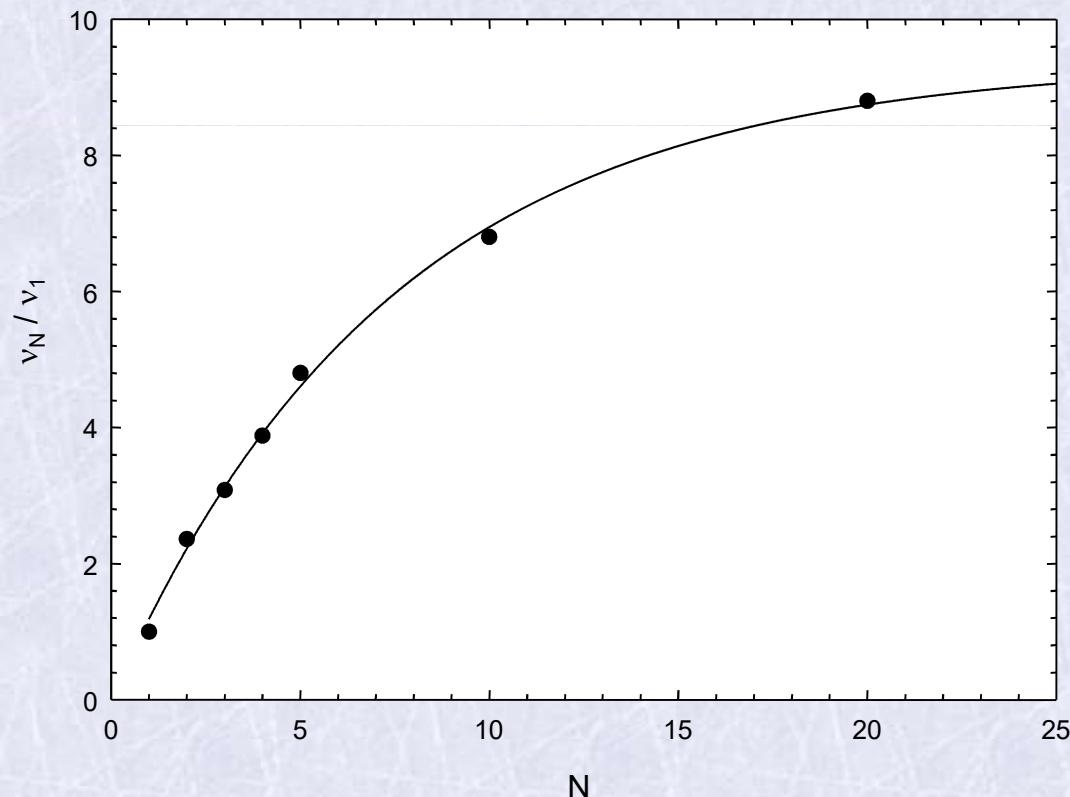
- vacancy clusters
- *ab-inito* calculations of positron lifetimes



## vacancy clusters

- specific positron trapping rates for vacancy clusters
- small clusters ( $N \leq 10$ ):  $\nu_N \sim N$
- larger clusters ( $N > 10$ ):  $\nu_N$  gradually saturates

*R. M. Nieminen, J. Laakkonen, Appl. Phys. 20, 181 (1979)*

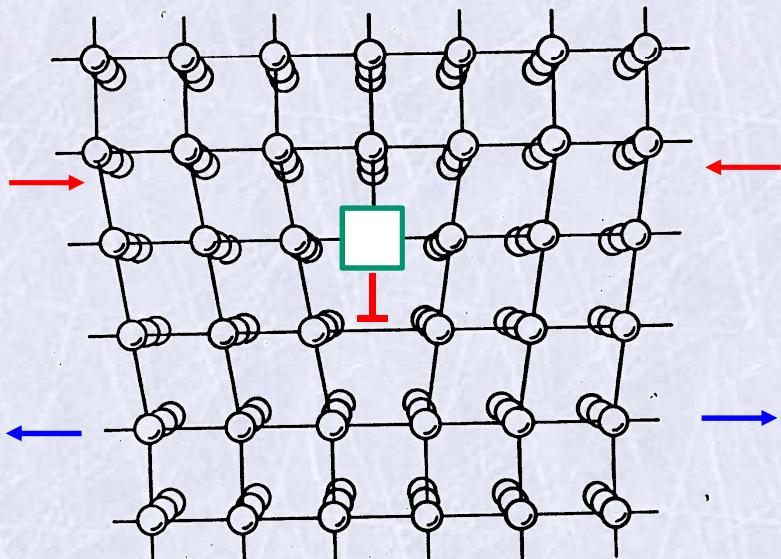


$$\nu_N / \nu_1 \approx a(1 - e^{-bN})$$
$$a = 9.4$$
$$b = 0.13$$

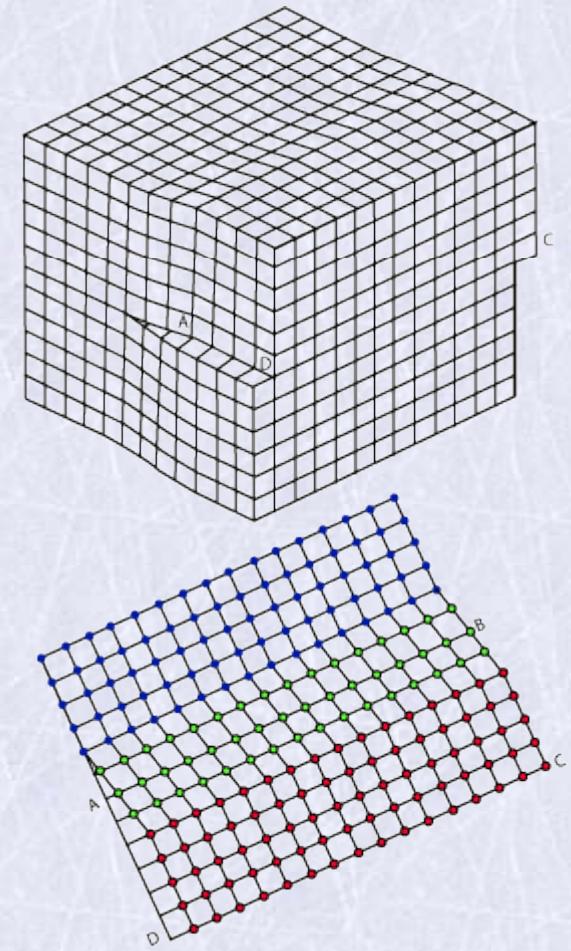
## Dislocations

- dislocation line is a shallow positron trap
- weak positron localization at dislocation → diffusion along dislocation line
- final trapping at vacancy bound to dislocation or open volume at jog

edge dislocation



screw dislocation

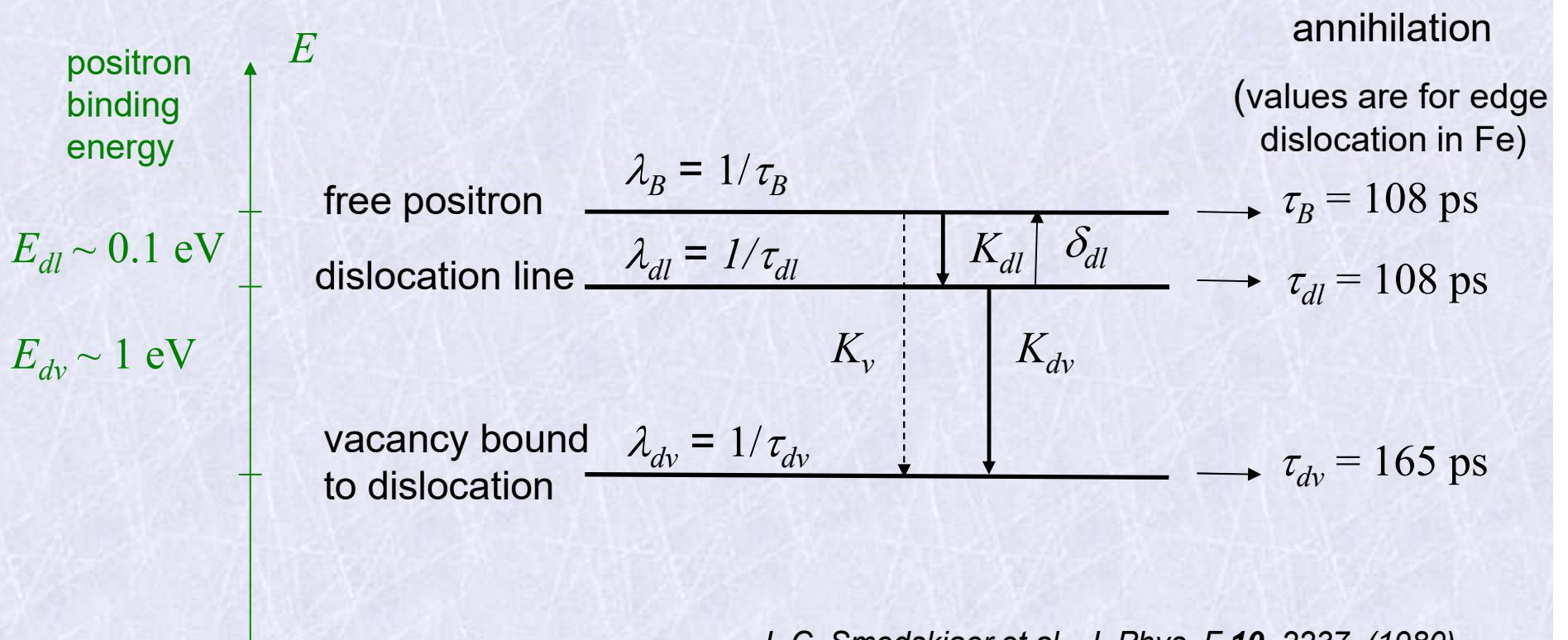


## Positron trapping at dislocations

- two-step positron trapping at dislocation

$K_v \ll K_{dl}$  (vacancy is a point defect but dislocation is a line defect)

$\delta_{dl} \ll K_{dv}$  (there is always enough vacancies attached to dislocation)



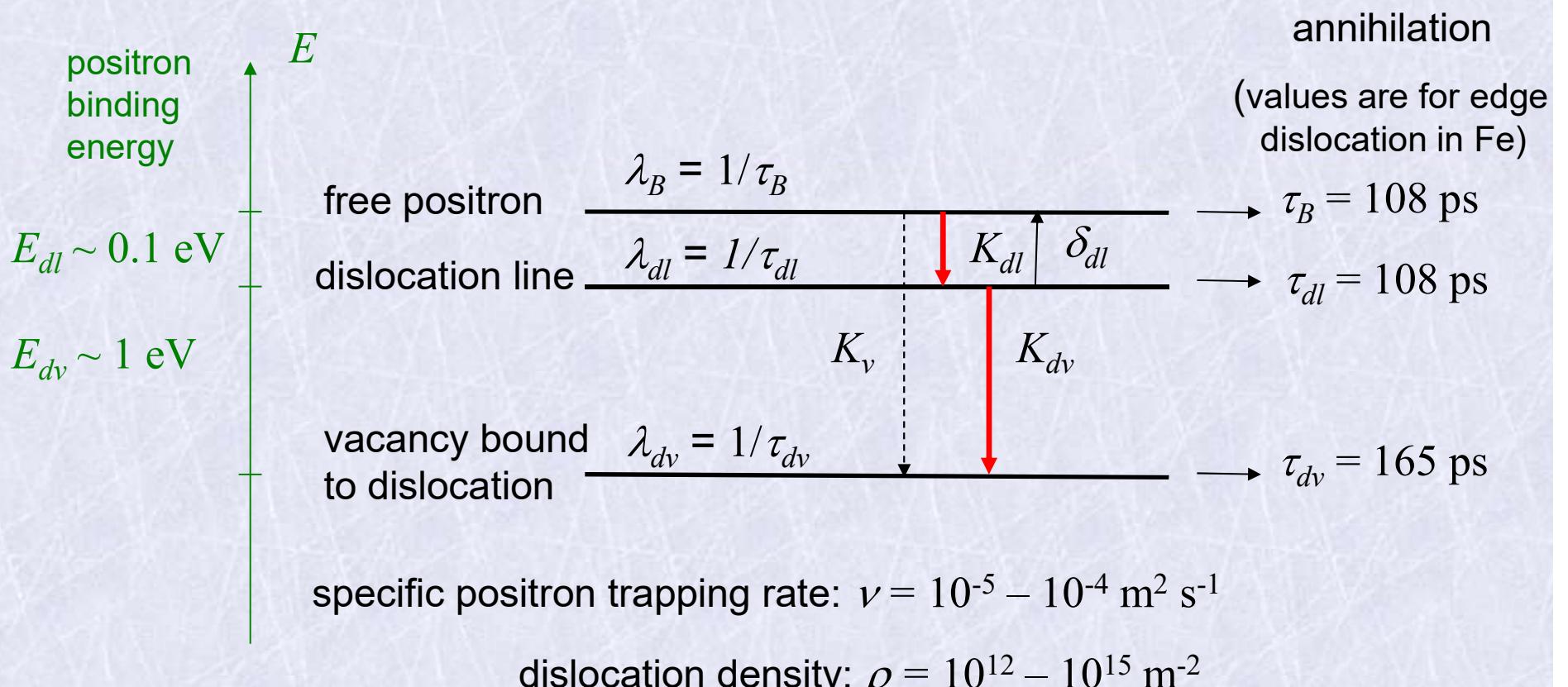
L.C. Smedskjaer et al., J. Phys. F 10, 2237, (1980)

## Positron trapping at dislocations

- two-state positron trapping at dislocation

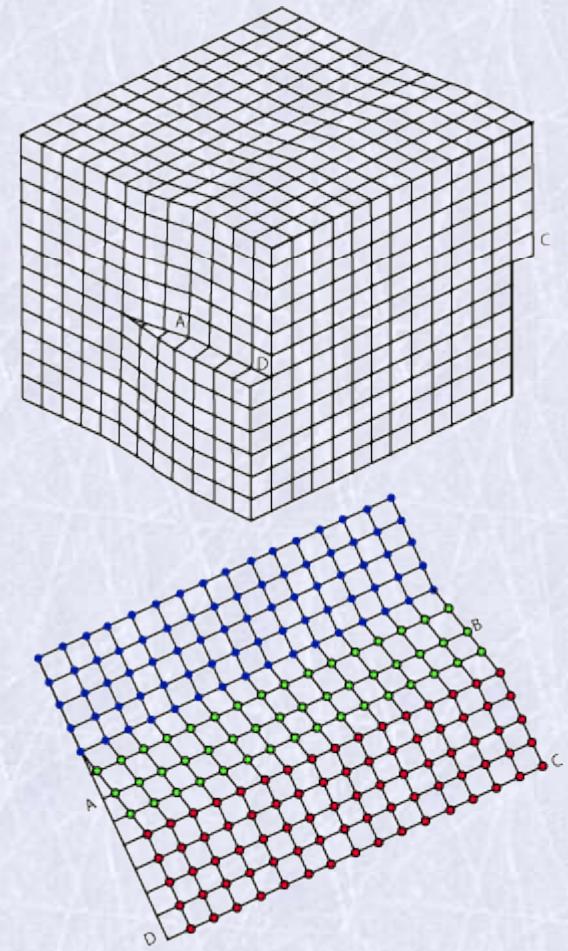
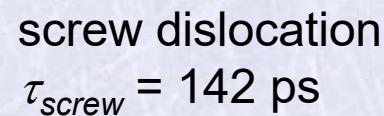
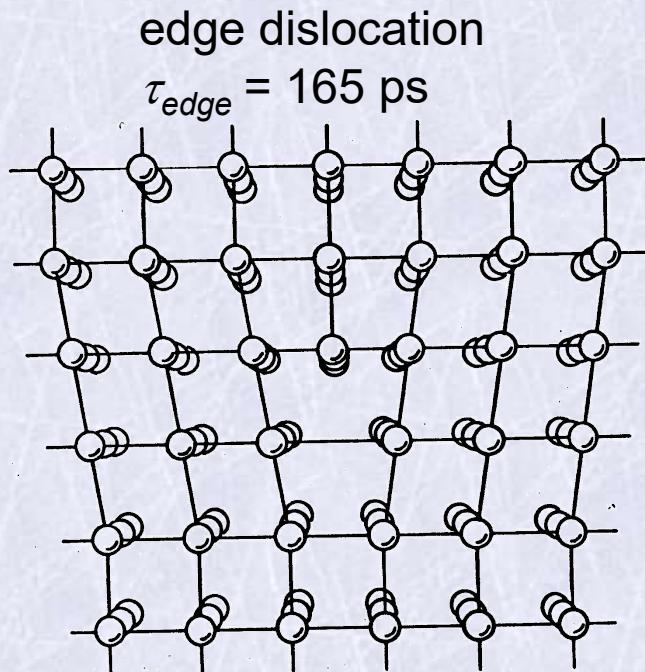
$K_v \ll K_{dl}$  (vacancy is a point defect but dislocation is a line defect)

$\delta_{dl} \ll K_{dv}$  (there is always enough vacancies attached to dislocation)



## Positron trapping at dislocations in Fe (or steels)

- open volumes attached to edge dislocations are larger Y.K. Park et al., PRB 34, 823 (1986)
- screw and edge dislocations can be distinguished

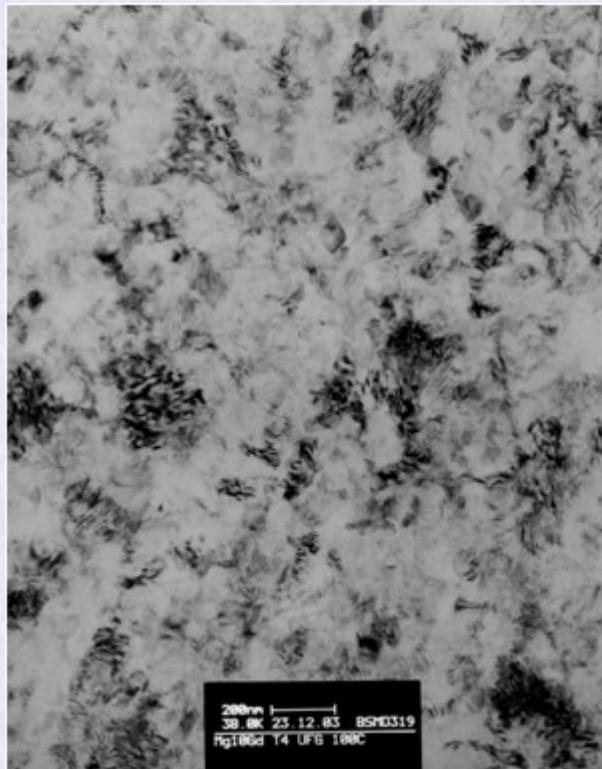


## Positron trapping at dislocations – distribution of dislocations

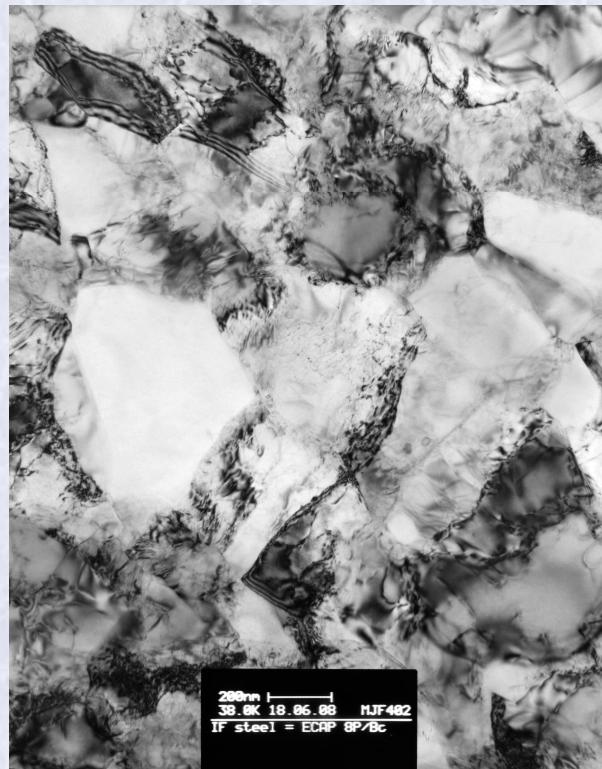
- uniform distribution of dislocations → simple trapping model  
(hcp metals, metals with low SFE)
- dislocation cell structure → diffusion trapping model  
(cubic metals with medium and high SFE)

$$\rho = \frac{1}{\nu} \frac{I_2}{I_1} \left( \frac{1}{\tau_B} - \frac{1}{\tau_D} \right)$$

↑  
specific positron trapping  
rate to dislocations



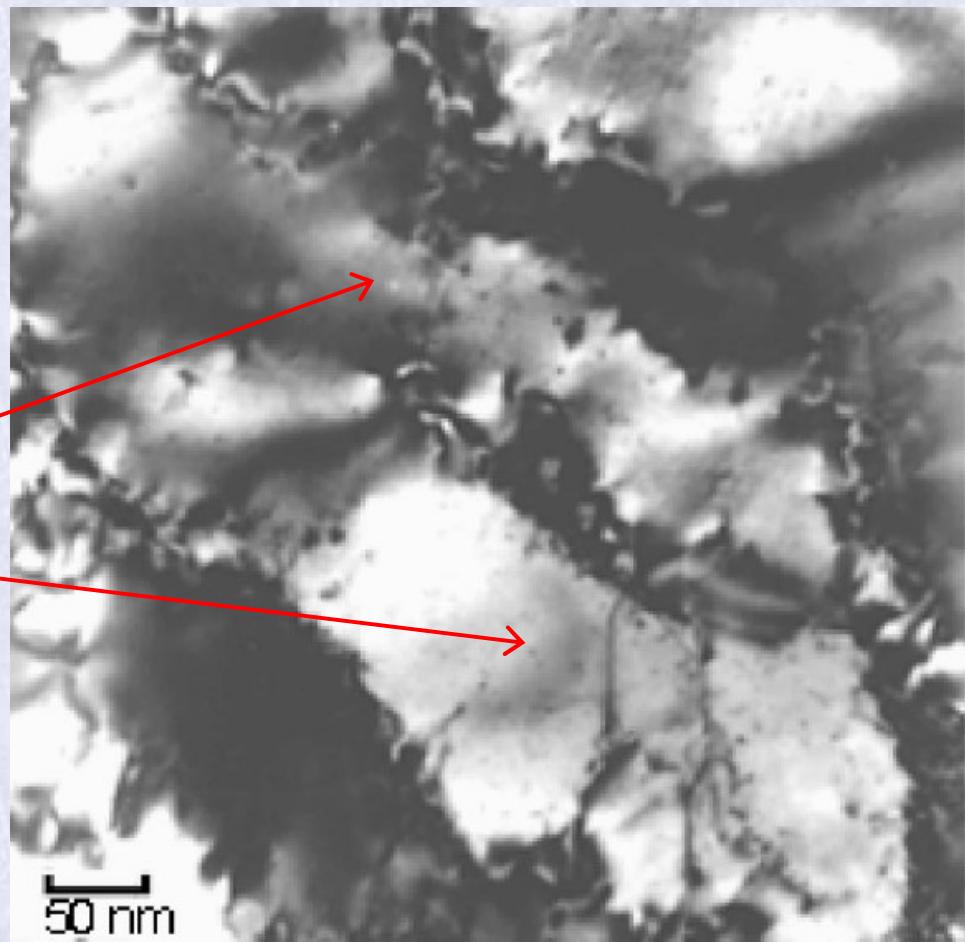
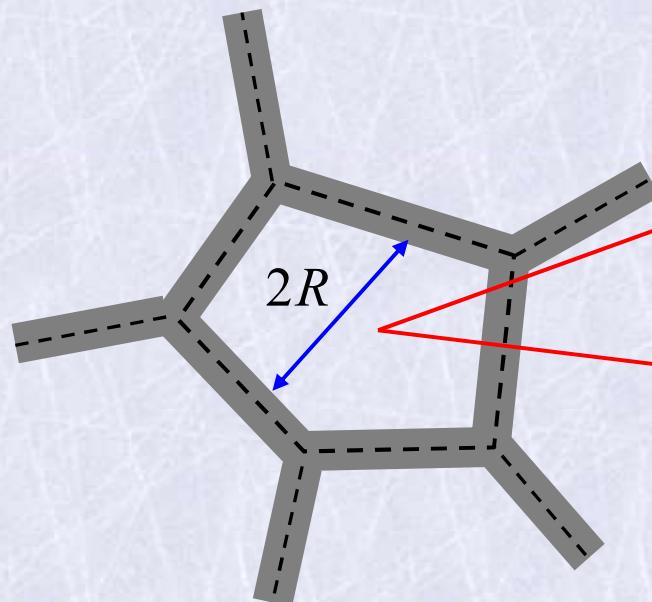
HPT-deformed Mg-10wt.%Gd alloy



HPT-deformed IF steel

## Positron trapping at dislocations – dislocation cell structure

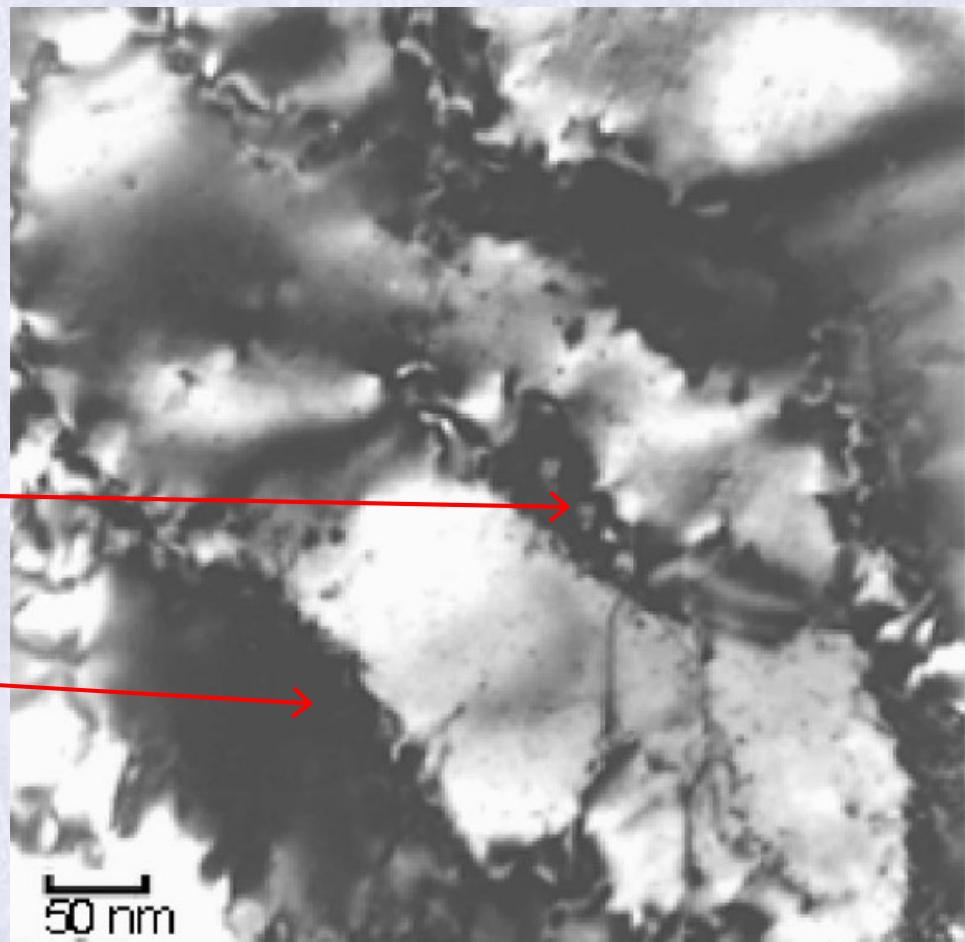
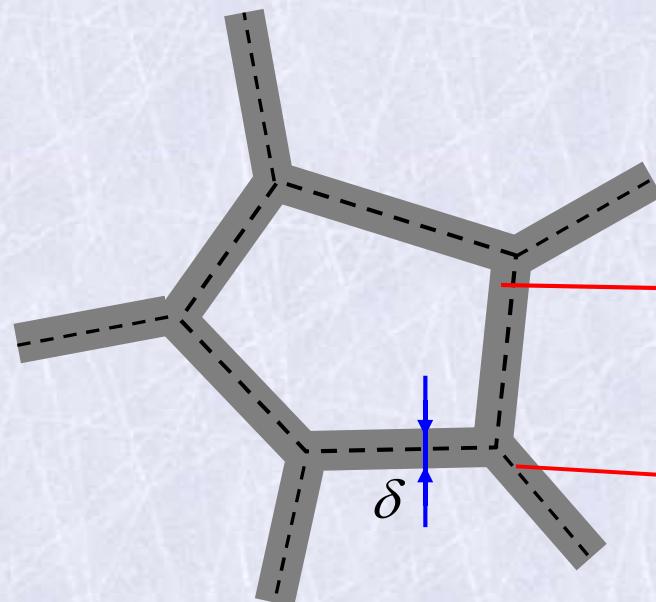
- dislocation cell structure
- dislocation-free cell interiors
- distorted regions with high density of dislocations (dislocation walls)



J. Čížek et al. Phys. Rev. B 65, 094106 (2002)

## Positron trapping at dislocations – dislocation cell structure

- dislocation cell structure
- dislocation-free cell interiors
- distorted regions with high density of dislocations (dislocation walls)



J. Čížek et al. Phys. Rev. B 65, 094106 (2002)

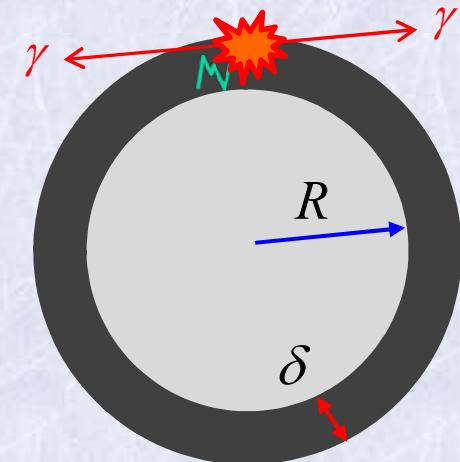
## Diffusion trapping model (DTM)

- dislocation-free spherical with radius  $R$
- surrounded by dislocation walls with thickness  $\delta$

thermalization



1.  $e^+$  stopped in dislocation walls  $\longrightarrow$  trapping at dislocations



A. Dupasquier et al. PRB **48**, 9235 (1993)

J. Čížek et al. PRB **65**, 094106 (2002)

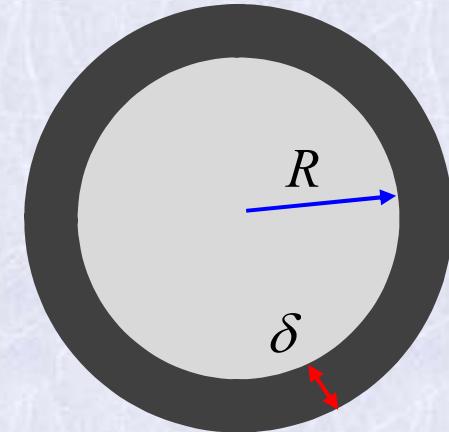
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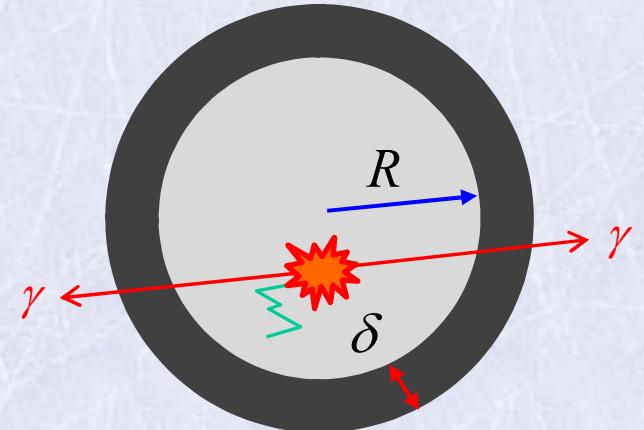
thermalization



1.  $e^+$  stopped in dislocation walls → trapping at dislocations

annihilation in  
delocalized  
state

2.  $e^+$  stopped inside cells



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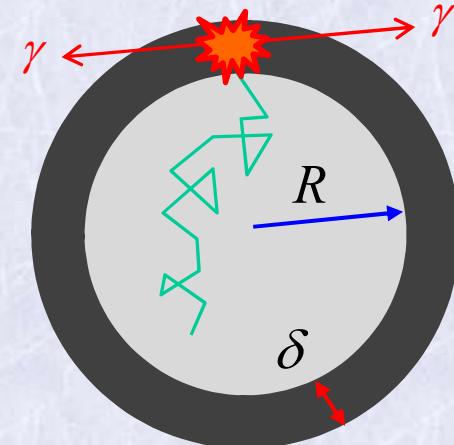
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annihilation in  
delocalized  
state

$$\frac{\partial n}{\partial t} = D_+ \left( \frac{\partial^2 n}{\partial r^2} + \frac{2}{r} \frac{\partial n}{\partial r} \right) - \lambda_B n$$

diffusion to dislocation walls

2.  $e^+$  stopped inside cells

$D_+$  - positron diffusion coefficient

$$\left( \frac{\partial n}{\partial t} \right)_{r=R} = - \frac{\nu \rho \delta}{D_+} n(R, t)$$

boundary condition

$$n(r, 0) = \frac{1 - \eta}{4/3 \pi R^3}$$

initial condition

$$\eta = \frac{(R + \delta)^3 - R^3}{(R + \delta)^3}$$

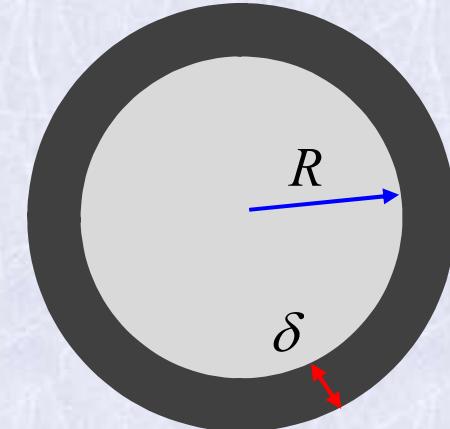
volume fraction  
of dislocation walls

A. Dupasquier et al. PRB **48**, 9235 (1993)

J. Čížek et al. PRB **65**, 094106 (2002)

## Diffusion trapping model (DTM)

- dislocation-free spherical with radius  $R$
- surrounded by dislocation walls with thickness  $\delta$
- positron lifetime spectrum



$$S(t) = \sum_k^{\infty} t_k^{-1} i_k e^{-t/t_k} + \tau_d^{-1} I_d e^{-t/\tau_d}$$

$\boxed{\tau_d}$  – lifetime of positrons trapped at dislocations

$$\boxed{I_d = 1 - \sum_k^{\infty} i_k} \text{ – intensity of dislocation component}$$

$$\boxed{t_k = \left( \tau_B^{-1} + \frac{\beta_k^2 D_+}{R^2} \right)^{-1}} \text{ – infinite number of free positron components}$$

$$\boxed{i_k = 3(1-\eta) \frac{\nu \rho \delta}{\eta R} \alpha_k \left( \frac{1}{t_k^{-1} - \tau_B^{-1}} - \frac{1}{t_k^{-1} - \tau_d^{-1}} \right)}$$

A. Dupasquier et al. PRB **48**, 9235 (1993)

$$\beta_k \cot \beta_k + \xi - 1 = 0$$

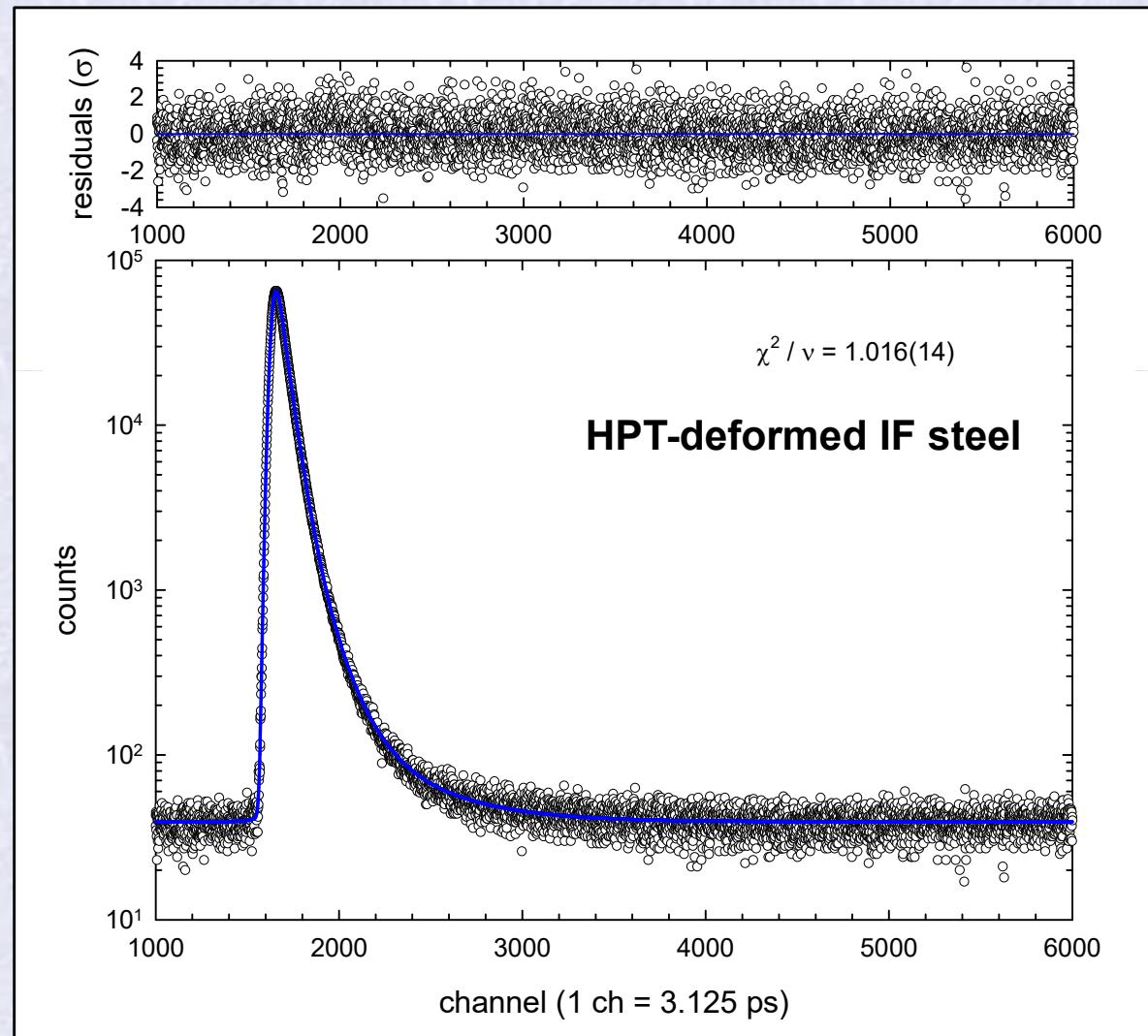
$$\alpha_k = \frac{2\xi}{\beta_k^2 + \xi(\xi-1)} \quad \xi = \frac{\nu R \rho \delta}{\eta D_+}$$

J. Čížek et al. PRB **65**, 094106 (2002)

## Diffusion trapping model (DTM)

- direct fitting of positron lifetime spectra by DTM
- from fitting we obtain the following structural parameters:

- size of cells  $2R$
- mean dislocation density  $\rho$
- volume fraction of distorted regions  $\eta$
- lifetime of positrons trapped at dislocations  $\tau_d$
- fraction of screw dislocations  $f_{screw}$



## Diffusion trapping model (DTM)

- direct fitting of positron lifetime spectra by DTM
- fixed parameters
- width of distorted regions  $\delta = 10 \text{ nm}$
- specific positron trapping rate to dislocations  $\nu = 0.36 \times 10^{-4} \text{ m}^2 \text{s}^{-1}$

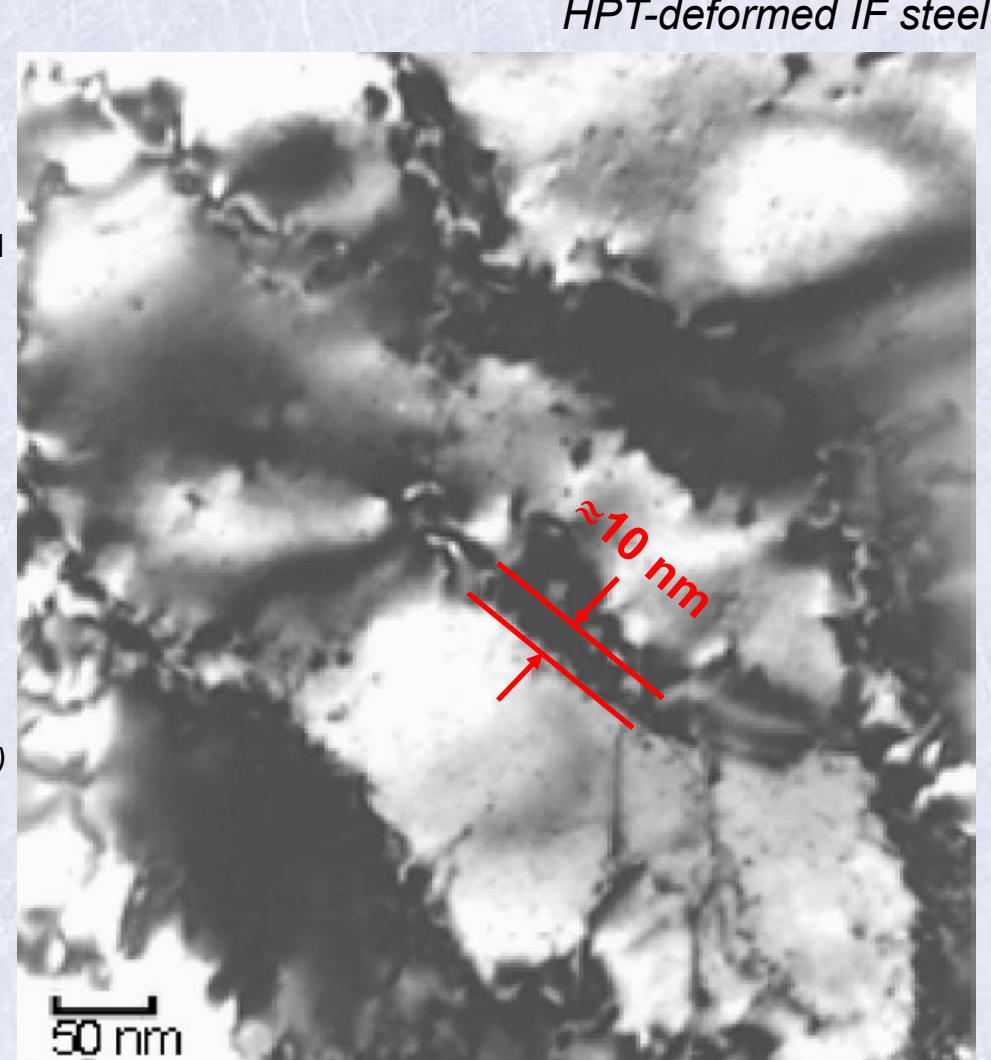
J. Čížek et al., *Phys. Stat. Sol. A* **178**, 651 (2000)

- bulk positron lifetime for Fe  
 $\tau_B = 108 \text{ ps}$

F. Bečvář et al., *Appl. Surf. Sci.* **255**, 111 (2008)

- positron diffusion coefficient for Fe  
 $D_+ = 1.87 \text{ cm}^2 \text{ s}^{-1}$

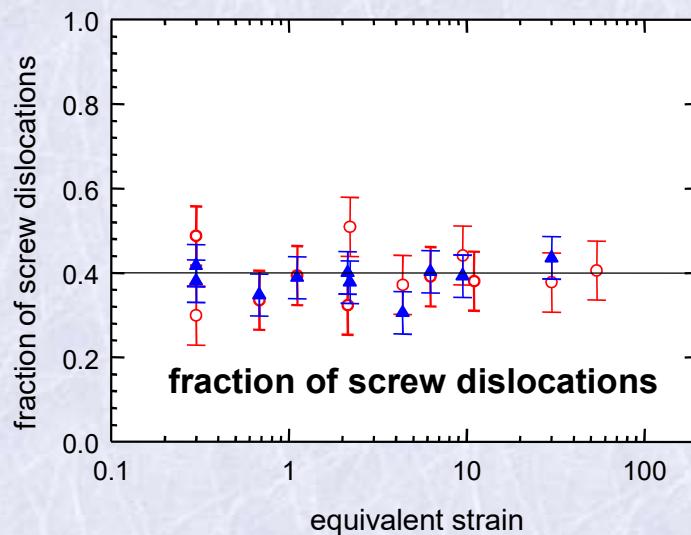
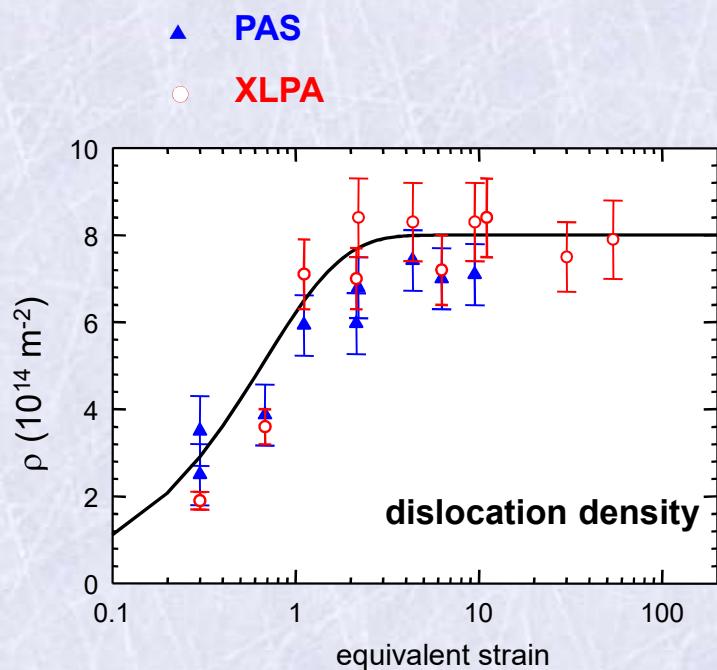
F. Lukáč et al., *J. Phys. Conf. Ser.* **443**, 012025 (2013)



## Diffusion trapping model (DTM)

### HPT-deformed steel

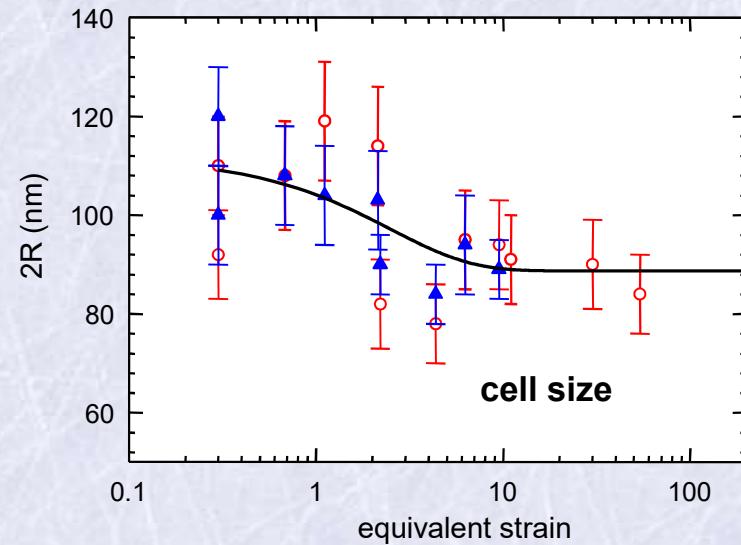
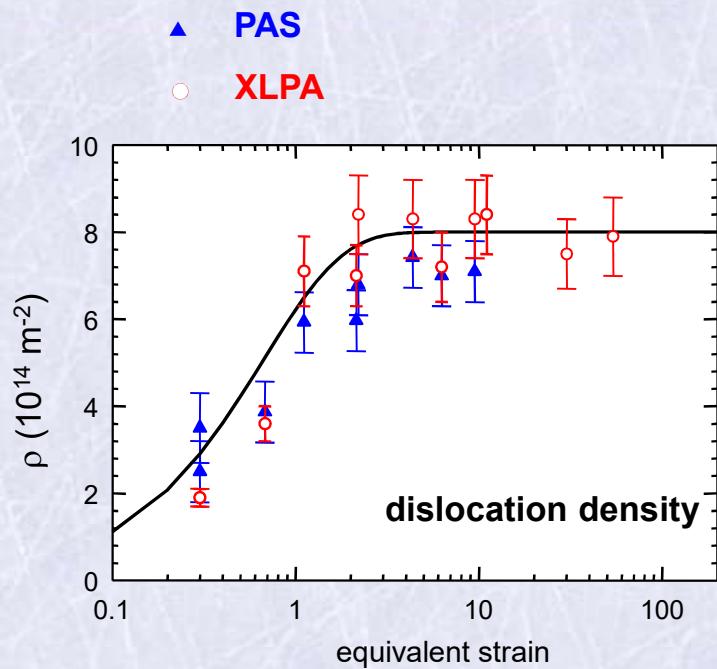
- good agreement of PAS and (XLPA = X-ray line profile analysis)
- dislocation density increases with deformation and saturates at strain  $e \geq 3$
- edge character of dislocations prevails



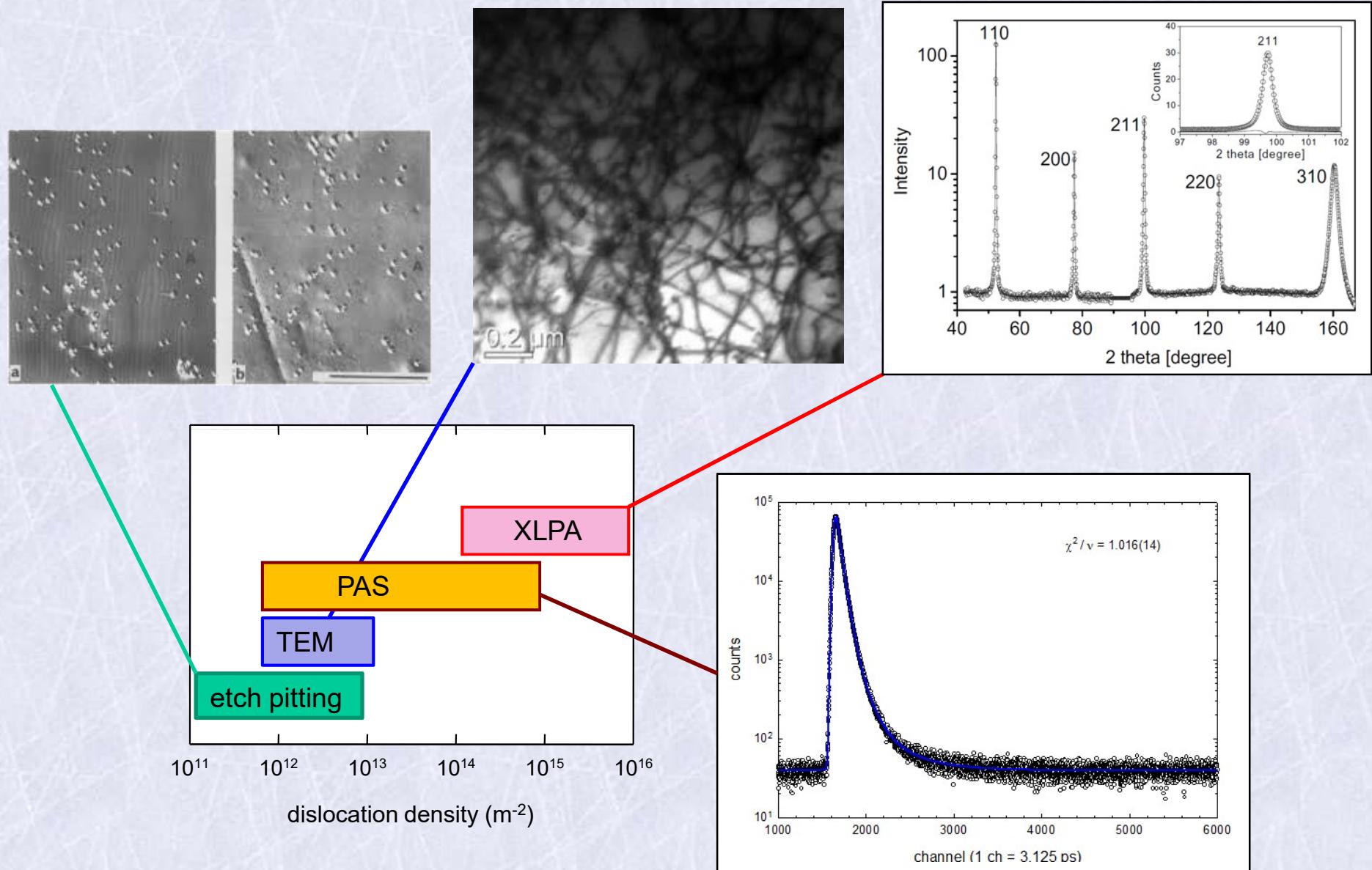
## Diffusion trapping model (DTM)

### HPT-deformed steel

- good agreement of PAS and (XLPA = X-ray line profile analysis)
- dislocation density increases with deformation and saturates at strain  $e \geq 3$
- edge character of dislocations prevails
- cell size saturates at  $e > 10$



## Dislocations – determination of dislocation density



dislocation density: total length of dislocation lines per unit volume

$$\rho = \sum l_{disl} / V$$

# SLOPOS -15

Prague, Czech Republic

September 2-6, 2019

See you in Prague

